TANAGER: Design and Validation of an Automated Spectrogoniometer for Bidirectional Reflectance Studies of Natural Rock Surfaces

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April 16, 2024

Abstract

Laboratory measurements of reflectance spectra of rocks and minerals at multiple viewing geometries are important for interpreting spacecraft data of planetary surfaces. However, efficiently acquiring such measurements is challenging, as it requires a custom goniometer that can accommodate multiple, bulky samples beneath a movable light source and detector. Most spectrogoniometric laboratory work to date has focused on mineral mixtures and particulates, yet it is also critical to characterize natural rock surfaces to understand the influence of texture and alteration. We designed the Three-Axis N-sample Automated Goniometer for Evaluating Reflectance (TANAGER) specifically to rapidly acquire spectra of natural rock surfaces across the full scattering hemisphere. TANAGER has its light source and the spectrometer’s fiber optic mounted on motorized rotating and tilting arcs, with a rotating azimuth stage and six-position sample tray, all of which are fully motorized and integrated with a Malvern PanAnalytical ASD FieldSpec4 Hi-Res reflectance spectrometer. Using well-characterized color calibration targets, we have validated the accuracy and repeatability of TANAGER spectra. We also confirm that the system introduces no discernable noise or artifacts. All design schematics and control software for TANAGER are open-source and available for use and modification by the larger scientific community.
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Laboratory measurements of reflectance spectra of rocks and minerals at multiple viewing geometries are important for interpreting spacecraft data of planetary surfaces. However, efficiently acquiring such measurements is challenging, as it requires a custom goniometer that can accommodate multiple, bulky samples beneath a movable light source and detector. Most spectrogoniometric laboratory work to date has focused on mineral mixtures and particulates, yet it is also critical to characterize natural rock surfaces to understand the influence of texture and alteration. We designed the Three-Axis N-sample Automated Goniometer for Evaluating Reflectance (TANAGER) specifically to rapidly acquire spectra of natural rock surfaces across the full scattering hemisphere. TANAGER has its light source and the spectrometer’s fiber optic mounted on motorized rotating and tilting arcs, with a rotating azimuth stage and six-position sample tray, all of which are fully motorized and integrated with a Malvern PanAnalytical ASD FieldSpec4 Hi-Res reflectance spectrometer. Using well-characterized color calibration targets, we have validated the accuracy and repeatability of TANAGER spectra. We also confirm that the system introduces no discernable noise or artifacts. All design schematics and control software for TANAGER are open-source and available for use and modification by the larger scientific community.
1. Introduction

Studying the composition and distribution of minerals on planetary bodies is critical to understanding their surface evolution. Across the solar system, key mineral identifications have been made using visible to near-infrared (VNIR) spectrometers on ground- and space-based telescopes, orbital spacecraft, and landers. VNIR reflectance spectroscopy relies on the analysis of diagnostic absorption features, specifically their band center wavelength positions, shapes, and depths (e.g., Bishop et al., 2020). However, VNIR reflectance spectra are not influenced by mineral composition alone. Variables such as grain morphology (size and shape), temperature, and nonlinear mixing effects also influence the shapes, positions and depths of diagnostic absorption features (e.g., Clark & Roush, 1984; Clark et al., 1999).

In particular, viewing geometry (photometric) effects can complicate remote sensing interpretations. Conversely, once understood, photometric effects can allow for richer inferences to be drawn than would otherwise be possible. For example, photometry has been used to constrain the microtexture of surface materials including roughness and porosity (e.g., Bandfield et al., 2015; Hapke and Sato, 2016; Shepard et al., 2017). Microtextural characteristics can in turn be used to understand surface processes (e.g., regolith/soil formation and evolution), to serve as inputs to planetary thermal models, and to constrain mechanical properties relevant to exploration. Such investigations have been performed for the Moon (e.g., Shkuratov et al., 1999), asteroids (e.g., Clark et al., 2002), Mars (e.g., Johnson et al., 1999; see also Fernando et al., 2015; Johnson et al., 2006a-b; Johnson et al., 2021, 2022; Lichtenberg et al., 2007) and other planets (e.g., Veverka et al., 1988; Schröder & Keller, 2009). Furthermore, several models have been developed to better understand how the microscale physical properties of surfaces influence photometry (e.g., Hapke, 1993; Shkuratov et al., 1999).
Photometric effects, however, are often not included in laboratory VNIR reflectance measurements of reference rocks and minerals. Many commercial VNIR spectrometers do not allow users to easily control the incidence and emission angles, and most laboratory spectra are acquired with a single, fixed geometry (e.g., incidence = 30°, emission = 0°). In contrast, telescopic and spacecraft observations of planetary surfaces are acquired at a variety of geometries, depending on the relative positions of the light source (Sun), target material (planetary surface), and detector (spectrometer/camera) (e.g., Figure 1). Custom-built goniometers (which control the orientations of the incidence light and spectrometer’s detector) are required, therefore, for reproducing photometric effects in the laboratory.

![Cartoon of viewing geometries relevant to spacecraft exploration of planetary surfaces, for the specific example of spectroscopy measurements by a rover on Mars. Geometries shown include emission angle e, incidence angle i, and azimuth angle \( \phi \). Phase angle g is the angle between e and i.](Image)

To date, such “spectrogoniometry” measurements have focused primarily on particulate samples of uniform grain size and composition (e.g., Pommerol et al., 2013; Shephard and...
Helfenstein, 2007) or two-phase mixtures (e.g., Pilorget et al., 2016; Stack & Milliken, 2015). A limited number of laboratory studies have acquired spectrogoniometric measurements for whole rocks (Guinness et al., 1997; Shepherd & Arvidson, 1999). However, the compounding effects of composition, alteration, microtexture, and viewing geometry on complex rock surfaces are still poorly understood. Working with natural rock surfaces in the laboratory poses several challenges. For example, bulky samples require a non-standard goniometer setup with an adjustable sample stage and large incidence and emission arms.

We have designed and built such a system for the Mars Lab at Western Washington University (WWU) in order to characterize the spectrogoniometry of a variety of rock and mineral samples. Specifically, WWU’s Mars Lab studies VNIR reflectance spectra of naturally-weathered rocks as analogs to the geologic materials encountered by the Mars Exploration Rovers (MERs), the Mars Science Laboratory (MSL) Curiosity rover, the Mars-2020 Perseverance rover, and future landed missions. The science needs of the Mars Lab necessitate rapid acquisition of spectra from large numbers of bulky samples. For efficiency in collecting large datasets at high angular resolution, it is important to use a motorized system for precise, repeatable positioning of the light source, detector, and sample. Furthermore, software is required to automate the goniometer and allow it to interface with the spectrometer collecting the data. While some aspects of this ideal system have been developed previously for other laboratories (e.g., Biliouris et al., 2007; Camon & Lemelin, 2024; Painter et al., 2003; Pilorget et al., 2016; Pontin et al., 2018; Shepard and Helfenstein, 2007), no fully-automated system (to our knowledge) exists for goniometry with a hyperspectral instrument for measuring a variety of whole rock samples.
Here, we describe WWU’s Three-Axis N-sample Automated Goniometer for Evaluating Reflectance (TANAGER). (The acronym TANAGER also has local significance, as the Western Tanager is a brightly colored bird native to Washington state.) TANAGER derives heritage from the WWU Mars Lab’s previous planar goniometer (Hoza & Rice, 2019), which allows for automated collection of spectra from multiple bulky samples at varying incidence and emission angles. TANAGER substantially improves upon the planar goniometer design with the capability to collect out-of-plane geometries (i.e., varying azimuth), which is necessary to characterize the full bidirectional reflectance distribution function (BRDF). In partnership with the Seattle-based engineering company First Mode, LLC, we designed and characterized TANAGER to support rapid and comprehensive spectrogoniometric studies of natural rock samples.

2. Performance Requirements

To enable rapid collection of reflectance spectra from multiple rock surface across the full scattering hemisphere – as well as rapid analysis of the spectrophotometric datasets – we defined the following top-level requirements for TANAGER:

1. **Scientific Purpose:** The system shall enable collection of VNIR spectra at a range of geometries relevant to spacecraft measurements.

2. **Sample Type:** The system shall enable measurement of bidirectional reflectance for natural, unprocessed samples.

3. **Time Efficiency:** The system shall enable the following 2 concepts of operations: “Quick Runs” (8 hour time limit), and “Detailed Runs” (168 hour time limit).

4. **Data Visualization:** The system shall provide a means of documenting and visualizing the collected spectra.
5. **Safety**: Use of the system shall not result in damage to people, the goniometer, or other equipment, facilities, or samples.

To meet these requirements, TANAGER’s high-level design (Figures 2-3) differs substantially from other spectrogoniometer systems, as we outline in Section 3.

*Figure 2. Schematic of TANAGER with major components labeled. For scale, the dimensions of the baseplate are 80 x 95 cm.*
Each top-level requirement yields multiple sub-requirements (Table 1). First Mode, LLC evaluated all requirements except for sub-requirements 1.13, 2.1, 2.2 and 2.4, which were evaluated at WWU upon delivery of TANAGER in Spring 2021 (see Text S1-S5). Every sub-requirement has been met except for the detector head not falling inside the incident light beam for $g \geq 20^\circ$ (sub-requirement 1.1). However, we find the small shadow cast at $g = 20^\circ$ to be acceptable, as it is outside the detector pointing (Figure S1). Eight of the sub-requirements were also reevaluated after 300 hours of TANAGER run time (Table S1), which yielded recommendations for long-term operations of the hardware (Table S6).

**Table 1: Summary of the sub-requirements for TANAGER, which derive from the top-level requirements listed in the text. All sub-requirements have been met except for 1.10 (which was met within an acceptable threshold, as discussed in the text).**

<table>
<thead>
<tr>
<th>Sub-Requirement</th>
<th>Description</th>
</tr>
</thead>
</table>
| 1.1 Range       | The system shall enable measurements with  
|                 | - azimuth from $0^\circ$ to $170^\circ$  
|                 | - emission from $-70^\circ$ to $70^\circ$  
<p>|                 | - incidence from $-70^\circ$ to $70^\circ$  |
| 1.2 Phase angle | The system shall enable measurements at phase angles from $10^\circ$ to $140^\circ$ |
| 1.3 Angular control | The system shall have knowledge and control of detector and light source with $1^\circ$ steps in all directions |
| 1.5 Pointing accuracy - light source | The center of the illuminated spot shall not deviate from the target point by more than $\pm 10%$ of the illuminated spot diameter |
| 1.6 Pointing accuracy - detector | The center of the detector spot shall not deviate from the target point by more than $\pm 10%$ of the detector spot diameter |
| 1.7 Light bulb operating lifetime | The light bulb shall have an operating lifetime of at least 100 hours |
| 1.8 Target plane indicator | The goniometer shall provide the user with a clear indicator of whether a surface is in the target plane |</p>
<table>
<thead>
<tr>
<th>Requirement</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.9 Proximity to light source</td>
<td>The detector head and fiber optic shall not come within 5 mm of the light source during normal operations</td>
</tr>
<tr>
<td>1.10 No incident light on detector</td>
<td>The detector head shall not be inside the incident light beam for $g \geq 20^\circ$</td>
</tr>
<tr>
<td>1.11 Signal drift from heating at small phase angles</td>
<td>At geometries with phase angles below $20^\circ$, the standard deviation for repeated measurements taken over the course of 4 minutes shall not be greater than 0.02</td>
</tr>
<tr>
<td>1.12 Noise</td>
<td>For both light and dark samples, noise measured against a Savitzky-Golay smoothed spectrum with window size = 19, order = 2 shall not exceed</td>
</tr>
<tr>
<td></td>
<td>● +/- .001 in mid-range (500-2400 nm) wavelengths</td>
</tr>
<tr>
<td></td>
<td>● +/- .005 for long (2400-2500 nm) and short (450-500 nm) wavelengths</td>
</tr>
<tr>
<td>1.13 Polarization artifacts</td>
<td>Polarization artifacts shall not be more than 0.1 for basalt (or a similar sample) at any geometry where azimuth $= 180^\circ$ or $0^\circ$</td>
</tr>
<tr>
<td>2.1 Detector spot size</td>
<td>The detector spot size on the sample shall have a diameter less than the size of the Spectralon puck at $\epsilon = 70^\circ$ (9.1 cm)</td>
</tr>
<tr>
<td>2.2 Light spot size</td>
<td>The brightest part of the light spot size shall be 0.5 cm to 3 cm in diameter at $i = 0^\circ$</td>
</tr>
<tr>
<td>2.3 Sample tray repeatability</td>
<td>Each of the 6 sample tray positions shall be repeatable to within +/- 1 mm</td>
</tr>
<tr>
<td>2.4 Sample tray vibration</td>
<td>Sample tray movements and vibrations from other actuators shall not disturb the positioning of rounded coarse sand grains in sample cups</td>
</tr>
<tr>
<td>2.5 Sample accommodation</td>
<td>The sample tray shall accommodate up to 5 cylindrical samples (9.1 cm diameter, 0 to 5.1 cm height) plus 1 Spectralon puck</td>
</tr>
<tr>
<td>2.6 Center-of-sample markings</td>
<td>The sample tray shall have marked center of sample points for each position</td>
</tr>
<tr>
<td>2.7 Large sample compatibility</td>
<td>The sample tray shall not interfere with the measurement of spectra for large (&gt;10 cm) samples</td>
</tr>
<tr>
<td>2.8 Irregular sample positioning</td>
<td>The sample tray shall enable 5 different wedge-shaped samples plus the Spectralon puck to be positioned each with a surface that is:</td>
</tr>
<tr>
<td></td>
<td>● In the target plane to within +/- 1 mm</td>
</tr>
<tr>
<td></td>
<td>● Parallel with the target plane to within +/- 5°</td>
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<tr>
<td></td>
<td>● Sample heights may range from 0-5 cm, diameters from 3-9 cm</td>
</tr>
<tr>
<td>3.1 Viewing Geometries</td>
<td>Actuators shall be capable of positioning incidence, emission, and azimuth as described in sub-requirement 1.1</td>
</tr>
<tr>
<td>3.2 Sample tray rotation speed</td>
<td>Sample tray movements shall occur at an average speed of at least $4^\circ$ per second</td>
</tr>
<tr>
<td>3.3 Viewing geometry adjustment speed</td>
<td>Incidence, emission, and azimuth movements shall occur at an average speed of at least $0.2^\circ$ per second</td>
</tr>
<tr>
<td>3.4 Automatic software startup</td>
<td>Software on the spectrometer computer and raspberry pi shall start automatically</td>
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<td>-------------------------------</td>
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<tr>
<td>3.5 Legacy software</td>
<td>Unless otherwise noted, software shall provide the same functionalities and experience as existing software</td>
</tr>
<tr>
<td>3.6 Iteration across a range</td>
<td>Software shall enable data collection while iterating at a set interval through a range of incidence, emission, and azimuth angles as described in sub-requirement 1.1</td>
</tr>
<tr>
<td>3.7 Goniometer visualization</td>
<td>Software shall provide a visualization showing the software's understanding of the current state of the 3D goniometer including incidence angle, emission angle, azimuth angle, and sample tray position</td>
</tr>
<tr>
<td>3.8 Communication speed (microcontroller)</td>
<td>Communicating commands to and from the microcontroller shall take no longer than 1 second</td>
</tr>
<tr>
<td>3.9 Communication speed (spectrometer computer)</td>
<td>Communicating commands to and from the spectrometer computer shall take no longer than 1 second</td>
</tr>
<tr>
<td>3.10 Time limit (limited run)</td>
<td>A limited run of data collection shall take no longer than 8 hours</td>
</tr>
<tr>
<td>3.11 Number of samples (limited run)</td>
<td>A limited run of data collection shall characterize 1 sample</td>
</tr>
</tbody>
</table>
| 3.12 Viewing geometries (limited run) | A limited run of data collection shall include the following geometries:  
  - For a single plane (az = 0°) measure e, i with 10° resolution  
  - Outside that plane - 30° azimuthal resolution, 5 geometries at each azimuth  
  - Leave out reciprocal and rotationally equivalent geometries |
| 3.13 Time limit (detailed run) | A detailed run of data collection shall take no longer than 168 hours |
| 3.14 Number of samples (detailed run) | A detailed run of data collection shall characterize 5 samples |
| 3.15 Viewing geometries (detailed run) | A detailed run of data collection shall include the following geometries:  
  - 30° azimuthal resolution  
  - At each azimuth, 10° angular resolution for incidence, emission |
| 3.16 Spectra per sample       | At each geometry, a measurement of a single sample shall consist of averaging 200 spectra |
| 3.17 Human operator time      | Setting up a run of data collection shall not require more than 60 minutes of time from a human operator |
| 4.1 Data processing/visualization | Software shall be capable of processing and plotting data sets of up to 5000 spectra |
| 4.2 Feature requests          | Additional features may be added |
| 5.1 Light source casing temperature | The temperature of the light source shall not exceed 60° C |
5.2 Securability
The sample tray shall be securable

5.3 Position detection
The goniometer incidence, azimuth, and emission positions and the sample tray position shall be detected at the start of operations

5.4 Collision avoidance
Software shall not allow incidence, emission, or azimuth arms to collide with each other

3. Design and Characterization

3.1 Incidence Arm and Light Source

The primary design difference between TANAGER and most existing goniometers is the use of rotating and tilting arcs instead of straight arms, with the addition of cylindrical bronze ~1.5 kg counterbalance weights to provide stability and require less torque from the motors (Figure 4). The TANAGER system enables incidence and emission angles of -70° to 70°, and stepper motors allow for automated, repeatable movements to defined geometries sampling the full scattering hemisphere. This range of angles is sufficient to characterize scattering behavior using the Hapke model (e.g., Schmidt and Fernando, 2015).

Using two green laser guides on the incidence arm (Figure 5), we can ensure that the surfaces of bulky samples are positioned precisely in the focal plane. The brightest portion of the illuminated spot size in the focal plane at \( i = 0° \) is 2.7 cm in diameter, and larger at higher incidence angles (but always <9.1 cm, per sub-requirement 2.2; Table 1). Because the illuminated spot size is not actively controlled, it is possible to measure slightly different portions of the sample surface at different incidence angles, especially with high emission angles where the detector spot (which is similarly not actively controlled) can be larger than the
illuminated spot. Users should take this into consideration for high phase angle measurements of non-uniform samples.

**Figure 4.** Schematic of TANAGER’s incidence arm. The diameter of the arc is 67 cm. Illumination is provided by a Thorlabs VNIR light source, and two bronze weights provide counterbalance. Two green laser guides intersect at the focal plane.

**Figure 5.** Green laser guides indicate when the sample is out of the focal plane (left) and within the focal plane (right, when two dots become one).

The apex of the incidence arm supports a Thorlabs SLS201L light source with integrated cooling system and peak output near 1000 nm (Figure 6). This commercial light was selected for its relatively long bulb lifetime, sufficient power output across the 400-2500 nm wavelength range, and minimal heating. We characterized heating on color standards and geologic targets in the focal plane (Text S1) and found the temperature increases to be minimal: Spectralon®, which
heated negligibly (0.4°C), and other targets’ temperatures increased by 2-4°C over typical exposure durations (~2 minutes of direct illumination during nominal TANAGER operations) (Figure S2). We also characterized the effects of incident light heating on adsorbed water by monitoring spectral changes to powdered anhydrite (CaSO₄) over time (Text S2). During 30 minute periods of exposure, we observed no changes to the hydration absorptions attributed to adsorbed water on grain surfaces (Figures S2-S4), which gives us confidence that the sample heating is too minimal to drive adsorbed water off mineral grains or otherwise dehydrate samples.

![Optical power: 500 mW](image)

*Figure 6. Thorlabs VNIR light source (left) with power distribution curve for a blackbody and as measured (right).*

3.2 Emission Arm

TANAGER interfaces with a Malvern PanAnalytical ASD FieldSpec4 Hi-Res reflectance spectrometer (hereafter, “FieldSpec”; Section 3.5), and its emission arm is designed to accommodate the fiber optic cable attached to the spectrometer (the reflectance probe). Like the incidence arm, the emission arm uses stepper motors for precise, repeatable positioning of emission angles from -70° to 70°. The design of the arm is an arc (Figure 7) with a collimating
lens that reduces the detector spot size at the focal point. Reflected light entering the collimator is directed to the fiber optic cable via an angled mirror at the end of the emission arm. We characterized how the detector spot size changes with emission angle (Text S3) and found a minimum of 1.6 cm at $e = 0^\circ$ and a maximum of 3.5 cm at $e = 70^\circ$ (Table 2). At small incidence angles, this means that the detector spot falls entirely within the illuminated portion of the sample for emission angles $< 50^\circ$.

**Figure 7:** Components of the emission arm’s tubing, which guides the position of the FieldSpec’s fiber optic cable and maintains a wide arc at all geometries.

**Table 2:** Detector spot size ranges measured for different emission angles (see Text S1).

<table>
<thead>
<tr>
<th>Emission angle (°)</th>
<th>Measured Spot Size Range (cm)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>1.6-2.0</td>
</tr>
<tr>
<td>15</td>
<td>1.8-2.6</td>
</tr>
<tr>
<td>30</td>
<td>1.8-2.2</td>
</tr>
<tr>
<td>50</td>
<td>2.4-2.8</td>
</tr>
<tr>
<td>70</td>
<td>2.8-3.5</td>
</tr>
</tbody>
</table>
The emission arm design ensures that the spectrometer’s fiber optic cable (the reflectance probe) does not bend in any geometry. A guide tube keeps the fiber in a repeatable position from one measurement to the next, which consists of a short, fixed portion close to the detector tip and a longer, rotating portion farther back (Figure 7). This tubing allows for the fiber optic to be easily removed and replaced when the FieldSpec needs to be detached from TANAGER (e.g., when used with a Malvern Panalytical Contact Probe or Small Diameter Probe). To prevent bending of the fiber optic, the system is designed to maintain a 35 cm diameter of curvature.

3.3 Azimuth Turntable

The incidence arm is mounted to a geared turntable which controls azimuth angle between $0^\circ$ and $180^\circ$ (Figure 8). The large gear ratio reduces the necessary torque and increases angular accuracy. The system includes a homing routine with stops installed onto the baseplate. One challenge in the azimuth design is the need to manage cables for the light source, incidence motor, and incidence encoder as azimuth changes. The solution in TANAGER’s initial design used the combination of slider, coiled cable, and spring-loaded arm to enable consistent motion across the azimuth range (Figure 9). However, upon extensive use in WWU’s Mars Lab, we found that the slider’s and spring arm’s motions were finicky, so we attached the coiled cable to a fixed lab surface with ample clearance instead (Figure 10).
Figure 8. Left: Schematic of the azimuth turntable mounted with the attachments and stepper motor for the incidence arm. Middle: Detail of gears for the azimuth turntable. Right: Schematic of the homing mechanism on the azimuth baseplate.

Figure 9. Initial cable management solution for the full range of azimuths (0° to 180°).
Figure 10. Final cable management solution for the full range of azimuths (0° to 180°).

3.3 Sample Trays

The goniometer design includes two stages for positioning samples within the focal plane. Both are motorized and can rotate up to five samples in and out of the field of view with a Spectralon® white reference correction at each geometry. The first is a single, height-adjustable surface designed for multiple samples of the same height (e.g., particulates in sample cups) or for a single, bulky hand sample (Figure 11). For use with this stage, we designed sample cups at the
same height as the white reference and risers for positioning Scanning Electron Microscope (SEM) mounted samples.

Figure 11. Left: Single-height, rotating sample stage. Right: Custom sample cups and risers for SEM mounts designed with the same height as the Spectralon® white reference puck.

The other stage consists of six pie-slice-shaped sample supports, each of which can be moved independently (height and tilt) to accommodate a variety of bulky samples (Figure 12). Many degrees of freedom are required for positioning a near-flat portion of each sample into the focal plane. Adjustable screws can be added/removed to keep samples in place, and multiple sample supports can be used to support a single, awkward sample (Figure 12 right). In characterizations of sample tray motion during TANAGER operations (Text S4), we found that vibration was undetectable during incidence and emission arm motions, and minimal during azimuth and tray motions (Figure S5). TANAGER’s movements are highly unlikely to change the positions of samples on the tray or shift loose material within sample cups (Figure S6).
Figure 12. Left: Schematic of the multi-height, rotating sample stage. Six independently-adjustable, pie-slice-shaped supports allow for the positioning of a variety of samples. Right: Example of a bulky, awkward sample positioned with a horizontal surface in the focal plane using two supports and stabilizer screws.

3.4 Paint

Before delivery of TANAGER, all components were coated with a matte black paint to minimize stray light reflections from the metallic surfaces. We collected VNIR spectra for a range of different black paint options (LabIR Paints, Rustoleum, Fusion, black30), and all exhibited similar spectral shapes and low albedos throughout the 400-2500 nm range. Specular properties for all materials were also similar. Thus, we looked to mechanical adhesion and wear and selected LabIR Paints (https://paints.labir.cz/en/) because it performed best in mechanical tests. We applied the black paint to TANAGER via aerosol (Figure 3).
3.5 Spectrometer Interface

Sample spectra (averages of 200 for each) are measured relative to a Spectralon® white reference target at each geometry and corrected for minor (<2%) irregularities in absolute reflectance and for small offsets at 1000 and 1830 nm where detector changeovers occur (e.g., Cloutis et al., 2008). The ideal white reference material would be a perfectly Lambertian reflector (scattering incident light equally at all viewing geometries); in practice, however, such a material does not exist, but the geometry-dependent reflectance properties of Spectralon® have been well-documented (e.g., Shaw et al., 2016). We have incorporated the published Spectralon® corrections for high phase angles from Bhandari et al. (2012), using a linear interpolation when needed, into the analysis software (Section 2.9).

Other challenges to the spectrometer interface occur at high phase angles, where the emergence of artifacts near 1100 and 1310 nm in spectra from FieldSpec and similar spectrometers have been documented (e.g., Buz et al., 2019) and shown to originate from polarization of the sample and probe (Levesque & Dissanaka, 2016). These polarization artifacts are challenging to correct, but fortunately, their wavelength positions do not interfere with the locations of the prominent spectral features and absorptions in rock-forming minerals and their alteration products. We quantified the strength of these artifacts for our prototype planar goniometer (Hoza & Rice, 2019), for a variety of materials at a range of phase angles, and found that they were consistently negligible (<1%) at phase angles between $g = -20^\circ$ and $g = 40^\circ$. Therefore, we designed an option to omit the region 1050-1350 nm from TANAGER’s high phase angle analyses, as done by Buz et al. (2019). However, we have rarely needed this option...
in practice, as TANAGER’s spectra rarely exhibit polarization artifacts (and, when they do appear, they are < 2%; Text S5; Figure S7).

3.6 Automation and Control Software

Automation is a critical design component of TANAGER. Our previous studies verified the need for an automated system: using our prototype planar goniometer (Hoza & Rice, 2019) with a simple control software, we found that our rate of data collection increased by almost an order of magnitude. When manually positioning targets and the goniometer arms, acquiring measurements at 10 viewing geometries with Spectralon® white reference correction took roughly 90 minutes for a single sample and required an attendant in the lab to adjust the goniometer and perform the white reference calibration every few minutes. However, with automation, we acquired spectra of five samples with white reference corrections at 10 viewing geometries each in under 60 minutes total, including time for data processing and plotting, with minimal need for supervision by a lab attendant (Hoza & Rice, 2019). For more detailed analyses requiring high angular resolution (~100 geometries), automation reduced the total acquisition time per sample from ~15 to ~2 hours.

For TANAGER, a total of four stepper motors drive the incidence, emission, azimuth, and sample tray components, as described above. First Mode, LLC designed custom software for TANAGER in open source packages called “tanager-feeder” (Hoza, 2023). The software operates three computers all connected to a local spectroscopy lab network (Figure 13):

1. *Control computer*. This is where the user gives input. Software running on this computer includes a Python Graphical User Interface (GUI) that allows the user to input all parameters relating to sample configuration, spectrometer configuration, and desired
viewing geometries. This GUI also displays information about the current state of the system (Figure 14) and includes a log of all actions taken during the current session.

2. Spectrometer computer. This computer is controlled via command files generated by the control computer and dropped into a shared folder on the local network. Following instructions in these command files, it runs GUI automation software that operates the proprietary spectrometer control software (RS3) and spectral processing software (ViewSpec Pro). This enables the instrument to be optimized and for a white reference taken at each viewing geometry. After each run of data collection, this spectral processing software is used to apply a splice correction to remove artifacts generated at the positions where spectrometer detectors overlap.

3. Raspberry Pi. This computer is also controlled via command files generated by the control computer and dropped into a shared folder on the local network. Following instructions in these command files, it operates the motors driving the goniometer arms and sample tray. The software is designed with safety in mind; for example, it keeps the emission and incidence arms out of harm’s way while other parts are rotating. The control system also notices if motorized parts are not making progress and stops and alerts the user via the control computer.
Figure 13. Panoramic photo of the lab containing TANAGER (upper left) showing the relative placements of the FieldSpec, Raspberry Pi, control laptop, and spectrometer computer. Blackout curtains are hung behind TANAGER in order to minimize stray light.

Figure 14. Screenshot of “tanager-feeder” control software GUI with settings on the left, visualization of current goniometer and sample stage configuration on the upper right, and command line interface at lower right.

3.7 Analysis Software

In addition to operating the goniometer and spectrometer, the “tanager-feeder” software includes a suite of tools that can be used to view and analyze spectrophotometric data. In the
simplest case, a selected set of spectra are plotted with wavelength on the x-axis in nanometers and reflectance (relative or absolute) on the y-axis (Figure 15a). Additional analytical capabilities include normalizing spectra to 1.0 at a given wavelength (Figure 15b); calculating spectral slope (defined as the change in relative reflectance divided by the change in wavelength in nm; Figure 16); calculating band centers and depths of features between user-defined shoulder wavelength positions (as defined by Clark, 1999); calculating average reflectance for all values between a given wavelength range; adding offset values to spectra for clarity (Figure 17); and excluding wavelength regions with known artifacts (Figure 18).

**Figure 15:** Example of spectra before (a) and after (b) normalization to 1.0 at wavelength 680 nm.
**Figure 16:** Spectral slopes are calculated from a range of wavelengths identified for spectra of interest (a) and can be plotted as a function of phase angle \( \phi \) (b). In this case, slopes are calculated from 550-950 nm and are shown to become less negative as phase angle increases.

**Figure 17:** Overlapping spectra (a) can be hard to interpret, but adding offsets to samples can add clarity (b).

**Figure 18:** Polarization artifacts can appear within wavelengths 1000-1400 nm at high phase angles (a), so these regions can be omitted from our results for given geometries and replaced with dashed lines (b). Spectra shown are from the WWU Mars Lab’s planar goniometer (Hoza & Rice, 2019); in practice, TANAGER spectra rarely exhibit polarization artifacts (Text S5; Figure S7).

When interpreting spectra taken at a wide range of geometries, alternative visualization techniques can be beneficial for displaying some photometric behaviors. For example, to show the shapes of scattering lobes for measurements in a single plane (fixed azimuth), two-dimensional hemispherical plots can be much more effective than the original spectra (Figure
Our software also allows fixed azimuth data to be displayed with a heatmap; in these plots, emission angle is on the x-axis, incidence angle on the y-axis, and a user-defined parameter (such as reflectance at a given wavelength, band depth of a specific features, etc.) is represented by a color scale (Figure 20). For three-dimensional datasets (including variations in azimuth angle), the software enables visualizations of spectrophotometric behaviors as scattering lobes and/or heatmaps (Figure 21).

**Figure 19:** Examples of two-dimensional hemispherical plots: (a) Reflectance is measured for three samples at an incidence angle of -20 degrees and emission angles varying from 0 degrees to 60 degrees. (b) Reflectance values at 680 nm are plotted on a hemispherical plot with reflectance on the radial axis and emission angle varying with theta. Spectra shown are of uncoated (blue, green) and silica-coated (red) basalt surfaces (Hoza, 2019).
Figure 20: Examples of two dimensional “heat map” plots: (a) Reflectance is measured at all viewing geometries for a given sample (incidence = -50° shown here). (b) Reflectance at 680 nm is plotted as a heat map in incidence, emission space with a color scale representing a range of reflectance. (c) For a different sample, slope from 550-950 nm is measured for normalized spectra at all viewing geometries (incidence = -50° displayed here). (d) Slope is then plotted on a heat map over incidence, emission space with the color scale corresponding to different slopes.
Figure 21: Examples of three-dimensional hemispherical plots of scattering patterns for the Spectralon® white reference (which is non-Lambertian above i = 45°), for reflectance values at 680 nm.

3.8 Operational Procedures

Approximately one hour of human operation time is required before TANAGER data collection can be initiated. A number of startup procedures are required to place and secure samples, perform safety checks, input run parameters, and generally ensure that data are collected safely and effectively. Below, we provide a high-level description of human-operator startup tasks for TANAGER data collection in “automatic mode”: 
1. **FieldSpec warmup**: Turn on the FieldSpec spectrometer to allow it to warm up for 60 minutes, as recommended by the manufacturer (ASD Inc., 2017).

2. **Sample positioning (initial)**: While the FieldSpec is warming up, perform the initial sample placements on the sample stage, level targets using a bubble level, and adjust the targets into the measurement plane with the indicator lasers (Figure 5). For larger, natural, or irregular samples, this may require significant manipulation of the sample tray stage and/or securing the sample with supports and stabilizer screws (Figure 12). Finally, test for collisions by manually moving the emission arm to +/- 50° (the steepest emission angle during sample tray rotation), rotating the sample tray 360°, and readjusting sample placement as necessary.

3. **Software setup**: After initial sample placement, turn on the Raspberry Pi, control computer, and spectrometer computer. In the user interface on the control laptop, configure the control computer interface to match the physical TANAGER set up, set the number of spectra to be collected, select the correct white reference calibration file, enter the desired geometries, and name the samples.

4. **Sample positioning (secondary)**: With Raspberry Pi on and the stepper motors engaged, recheck the sample placement, leveling, height, and collision risk for each sample and make final adjustments as necessary.

5. **Data collection**: During data collection, light sources unrelated to data collection (e.g. overhead lights and unnecessary computer monitors) should be turned off. A human operator may either remain in the lab (e.g. for a short run of 30 minutes) or leave the lab for the duration of the run (e.g. for multi-day runs) in order to
eliminate stray light from outside the lab. Western Mars Lab uses an infrared webcam to monitor the control computer software and TANAGER hardware for run completion or unexpected errors when the human operator is not in the lab.

4. Data Validation

4.1 Cross-Calibration

We validated TANAGER’s data quality by reproducing measurements of calibration target (“caltarget”) materials from Buz et al. (2019). The caltargets are a set of exceptionally well characterized color standards and are the reference targets for the Mastcam-Z instrument on the NASA Mars 2020 Perseverance rover (Kinch et al., 2020). These caltargets have also been used in the calibration of Mastcam-Z’s legacy instruments: Mastcam on the NASA Mars Science Laboratory Curiosity rover (Bell et al., 2017) and Pancam on the NASA Mars Exploration Rovers (Bell et al., 2006). The eight caltargets include AluWhite from Avian Technologies LLC; and Cyan, Green, Red, Yellow, Gray33, Gray70, and Black from Lucidion Inc.. Spectra from each target were collected at same geometries of Buz et al. (2019) and evaluated at subset of phase angles: backscattering geometry (i = 30°, e = 45°, az = 0°, g = 15°), standard geometry (i = 0°, e = 30°, az = 0°, g = 30°), specular geometry (i = -30°, e = 30°, az = 0°, g = 60°), forward scattering geometry (i = -45°, e = 30°, az = 0°, g = 75°), and very forward scattering geometry (i = -70°, e = 58°, az = 0°, g = 128°). Relative root mean square error (RMSE, defined in Text S3) was calculated to compare datasets. We consider a relative RMSE of 5% or less to be an acceptable threshold of error (as is the case in the radiometric calibration of flight hardware such as Mastcam-Z; Hayes et al., 2021).
Spectra from TANAGER agree with those from Buz et al. (2019) to within 0.05 reflectance units for the color and black standards, and to within 0.01 for the grayscale standards, in all geometries except for the highest phase angles (Figures 22-23 and Figures S8-S9). Wavelengths near 1100 nm and 1300 nm typically have large residuals (e.g., Figure 23 gray), which we attribute to known polarization artifacts that are prominent in the data from Buz et al. but nearly absent in TANAGER spectra (see Text S5). We also observe structure in the residuals near 1900 nm (e.g., Figure 22), where there is an H₂O absorption; Buz et al. (2019) note variations in this band strength in their spectra which they attribute to water in the instrument path length, and they recommend caution when interpreting small fluctuations in this region.

We observe the same general scattering behaviors for all targets as those reported by Buz et al. (2019): the brighter samples (light gray, red, cyan and yellow) are quasi-isotropic, the AluWhite sample is weakly backward scattering, and the darker samples (black, dark gray and green) are strongly forward-scattering. TANAGER spectra of the brighter samples suggest they are more isotropic than demonstrated by Buz et al. (2019) (i.e., TANAGER spectra show less variation in reflectance at high phase angles; Figure 22, Figure S8). The two highly forward-scattering geometries (i = 30° and e = -58°, -70°) show reversed behavior in TANAGER spectra compared to Buz et al. (2019); however, the TANAGER spectra are more consistent with the known scattering behaviors for these targets (e.g., the e = -70° spectrum is higher reflectance than the e = -58° spectrum for strongly forward-scattering targets; Figure 23, Figure S9). Therefore, the discrepancies between the two labs’ datasets may indicate improvements in TANAGER spectra over the previously-published versions.
Figure 22: Spectra of the cyan and red Mastcam-Z caltarget witness samples at multiple viewing geometries from TANAGER (top) compared to Buz et al. (2019) (middle), with residuals (bottom). All measurements were acquired at $i = 30^\circ$ and $az = 0^\circ$. 
Figure 23: Spectra of the light gray (70% white) and black Mastcam-Z caltarget witness samples at multiple viewing geometries from TANAGER (top) compared to Buz et al. (2019) (middle), with residuals (bottom). All measurements were acquired at $i = 30^\circ$ and $az = 0^\circ$. 
To minimize differences in absolute reflectance and focus on differences in spectral shape, we also normalized spectra to 1.0 at 754 nm and calculated relative RMSE at a representative range of geometries. The normalized spectra (Figure 24) have only minor differences in spectral shape and slope (except for the light gray target at $g = 128^\circ$). Relative RMSE values (Table 3) are less than 5% with two exceptions: (1) the black target and (2) highly forward-scattering geometries. We attribute the black target’s high relative RMSE to its dark albedo and low signal-to-noise, so we do not find these values concerning, but recommend caution when interpreting subtle spectral shapes in TANAGER spectra of dark materials.

The high relative RMSE values for the very forward-scattering geometry ($g = 128^\circ$) may result from differences between the Buz et al. (2019) and TANAGER lab setups. At the highest measurable phase angles, it is possible that TANATER’s detector may receive stray light reflected from lab walls and cabinets at high emission angles. To test and potentially mitigate scattered light effects, we hung blackout curtains on the surfaces immediately adjacent to TANAGER (shown in Figure 13) and recollected the $g = 128^\circ$ spectra, which led to general decreases in overall reflectance (Figure S10) and improvements in relative RMSE values (Table 3). We now hang black curtains over all surfaces adjacent to TANAGER as part of our standard procedure.
Figure 24: Spectra normalized to 754 nm of select caltargets from TANAGER (darker lines) and Buz et al. (2019) (lighter lines) at a range of viewing geometries. Minor artifact peaks are marked in the Gray70 and Black Buz et al. (2019) spectra for $g = 75^\circ$ and $g = 128^\circ$.

<table>
<thead>
<tr>
<th></th>
<th>g = 15°</th>
<th>g = 30°</th>
<th>g = 60°</th>
<th>g = 75°</th>
<th>g = 128°</th>
<th>g = 128° (with black curtains)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Cyan</td>
<td>3.9%</td>
<td>1.9%</td>
<td>1.2%</td>
<td>1.3%</td>
<td>9.0%</td>
<td>4.4%</td>
</tr>
<tr>
<td>Green</td>
<td>4.3%</td>
<td>1.9%</td>
<td>2.0%</td>
<td>2.2%</td>
<td>8.0%</td>
<td>4.1%</td>
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<tr>
<td>Red</td>
<td>1.9%</td>
<td>1.3%</td>
<td>1.4%</td>
<td>1.8%</td>
<td>2.8%</td>
<td>2.9%</td>
</tr>
<tr>
<td>Yellow</td>
<td>1.6%</td>
<td>1.3%</td>
<td>1.4%</td>
<td>1.7%</td>
<td>3.6%</td>
<td>4.6%</td>
</tr>
</tbody>
</table>
Table 3: Relative RMSE comparing spectra normalized to 754 nm from Buz et al. (2019) and TANAGER at a range of geometries for cross calibration. Green squares have RMSE <1%, yellow-green between 1% and 3% RMSE, orange between 3% and 5% RMSE, and red above 5%. “Blackout” RMSE, right, compares Buz et al. (2019) spectra to TANAGER data collected with the addition of blackout curtains in the laboratory.

4.2 Repeatability

The repeatability of TANAGER spectra was assessed through multiple measurements of the caltarget materials at the geometries specified in Buz et al. (2019): we compared two sets of spectra collected with TANAGER in November 2022 and February 2023. The gray and black targets have residuals < 0.01 reflectance units for all spectra except at the largest phase angles, and color target spectra are generally repeatable to within 0.02 reflectance units (Figures S11-S14). To assess repeatability of spectral shapes (as opposed to absolute reflectance), we also normalized the spectra to 1.0 at 754 nm to calculate relative RMSE (as in Section 4.1). All target-geometry combinations fall well below our 5% relative RMSE threshold, with 29 of 35 target-geometry combinations below 1% RMSE (Table 4). The very forward scattering geometry is less consistent than other geometries, but overall the data show remarkable reproducibility.
Table 4: Relative RMSE comparing duplicate runs on TANAGER normalized to 754 nm for the Calitargets at a range of geometries. Green squares have RMSE <1%, yellow-green between 1% and 3% RMSE, and orange between 3% and 5% RMSE.

To test repeatability of spectral measurements of heterogeneous, geologic surfaces, we collected duplicate spectra at a range of phase angles from a set of four naturally-coated basalt samples from Hawaii Volcanoes National Park. All samples were collected from the Puna Coast and Mauna Iki Trails (Theuer et al., 2024) and all have brightly-colored coatings in a mottled pattern, except for MIT_LC, which has a more uniform reflective and chatoyant coating over fine-scaled flow textures (Figure 25). We documented the placement and orientation of each sample, which we referenced while resetting samples between the first and second set of spectra.

Figure 25: Heterogeneous, naturally-coated basalts samples used to test TANAGER’s measurement repeatability.
Data from the two runs reproduce the same spectral shapes and scattering behaviors: the samples are highly forward-scattering, with substantially higher reflectances and more positive near-infrared slopes at $g = 128^\circ$ (Figure 26, Figure S15). For absolute reflectance spectra,
residuals for most geometries are < 0.005 reflectance units. For spectra normalized to 1.0 at 754
nm, the two datasets have a relative RMSE of 3% or below (Table 9). The one exception is for
the dark sample MIT_LC in the backscattering geometry, which has very low reflectance values
(Figure S15). The reproducibility of TANAGER spectra for these samples gives us confidence in
the consistency of both the spectrogoniometer’s performance and our sample staging procedure.

<table>
<thead>
<tr>
<th></th>
<th>g = 15°</th>
<th>g = 30°</th>
<th>g = 60°</th>
<th>g = 75°</th>
<th>g = 128°</th>
</tr>
</thead>
<tbody>
<tr>
<td>PCT_RC</td>
<td>0.6%</td>
<td>0.4%</td>
<td>1.0%</td>
<td>1.1%</td>
<td>0.4%</td>
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<tr>
<td>PCT_YC</td>
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<td>1.0%</td>
<td>1.1%</td>
<td>3.0%</td>
<td>1.1%</td>
</tr>
<tr>
<td>MIT_LC</td>
<td>5.6%</td>
<td>2.3%</td>
<td>2.1%</td>
<td>3.0%</td>
<td>2.1%</td>
</tr>
<tr>
<td>MIT_BC_2</td>
<td>2.1%</td>
<td>2.9%</td>
<td>2.2%</td>
<td>2.8%</td>
<td>0.6%</td>
</tr>
</tbody>
</table>

Table 9: Relative RMSE comparing duplicate runs on TANAGER normalized to 754 nm for four coated
basalt surfaces at a range of geometries. Green squares have RMSE <1%, yellow-green between 1% and
3% RMSE, orange between 3% and 5% RMSE, and red >5% RMSE.

5. Science Applications and Data Sharing

Our preliminary science analyses have utilized TANAGER’s unique design for rapid
spectral measurements for large suites of natural rock surfaces, either at a single “standard”
geometry (Rice et al., 2023) or over the full scattering hemisphere (Curtis, 2022; Theuer et al.,
2024). Other initial studies include characterizations of multi-phase mineral mixtures (Lapo et
al., 2023) and synthetic rock coatings on slabs (Gabbert et al., 2023) and sands (Gabbert et al.,
2024). Because TANAGER’s sample tray also accommodates SEM-mounted samples, we can
easily correlate spectrogoniometric measurements with microtextural properties from
backscattered electron (BSE) images and surface topography measurements (Duflot et al., 2022).

Ongoing work in the WWU Mars Lab will continue to exploit TANAGER’s capabilities
for interrogating natural rock surfaces. More generally, we anticipate that TANAGER’s design
can be useful for a variety of investigations, such as determining the bidirectional reflectance
distribution function (BRDF) and deriving optical constants of minerals (e.g., Lucy, 1998; Sklute et al., 2015). We hope other laboratories will adapt TANAGER’s open-source design (Hoza et al., 2023) and software (Hoza, 2023) for their own niche analyses (see Data Availability Statement).

When spectral datasets from TANAGER are published in peer-reviewed studies, we will make them available via VISOR (the [V]isible and [I]nfrared [S]pectroscopy br[o]wse[r], https://westernreflectancelab.com/visor/), an online data sharing and spectra visualization tool developed by Million Concepts, LLC in partnership with the WWU Mars Lab (Million et al., 2022). VISOR allows users to search for spectra from TANAGER and/or other published spectral databases, download spectra with associated metadata (viewing geometry and sample information), and dynamically plot user-selected spectra. Plotting capabilities include adjusting axes, normalizing spectra, applying offsets, measuring selected band depths and other spectral parameters, and convolving to the bandpasses of spacecraft multispectral cameras. We will also archive all published TANAGER datasets via third party repositories (e.g., https://zenodo.org/ or https://cedar.wwu.edu/) with a digital object identifier (DOI) and persistent identifier link.

6. Conclusions

TANAGER is a custom spectrogoniometer which is fully automated and integrated with a Malvern PanAnalytical ASD FieldSpec4 Hi-Res reflectance spectrometer. We defined TANAGER’s performance requirements to enable rapid, automated spectral data collection across the full scattering hemisphere for multiple, bulky rock samples with natural surfaces. In a detailed characterization of TANAGER’s performance, all defined requirements have been met. We reevaluated a selection of the performance sub-requirements after ~300 hours of use and
found only minor changes to the system; we recommend frequent monitoring of some
components, including laser guides and sample tray motors.

Using well-characterized color calibration targets, we have validated the accuracy of
TANAGER spectra in comparison to published data. TANAGER spectra match those published
from other spectrogoniometers within 5% relative RMSE, except for very low-albedo targets. In
repeated TANAGER data collection runs for the same samples, we confirm that TANAGER
spectra are self-consistent to within 2% in almost all instances. We also confirm that the system
introduces no discernable noise or artifacts; in fact, TANAGER improves the polarization
artifacts from ~1000 nm to 1400 nm that commonly occur in FieldSpec data at high phase
angles. Furthermore, we find that TANGER’s light source causes only minimal sample heating
(+2 to 4°C over typical exposure durations) and is highly unlikely to influence sample properties
such as hydration state.

The advantages of TANAGER’s unique design include automation for rapid data
acquisition, highly customizable viewing geometries, accommodation of multiple and/or
bulky/irregular samples, and easy transfer to SEM for correlation with surface textural and
compositional properties. For our near-term science analyses, TANAGER will primarily be used
to characterize the surfaces of naturally-weathered rocks as analogs to the martian surface;
however, TANAGER can be utilized for a variety of applications in reflectance spectroscopy.

We encourage other investigators to use and/or modify TANAGER’s open-source design and
software for their laboratories’ needs.
Acknowledgements

This work was funded as part of a NASA Solar System Working Program grant. We thank the staff of First Mode, LLC for their support in all stages of this project, including Peter Illsley, Elizabeth Frank and Sophia Kim. Western Washington University’s College of Science and Engineering, Geology Department, and Machine Shop supported laboratory renovations to accommodate TANAGER. We also thank Chase Million and Michael St. Clair of Million Concepts, LLC for development and ongoing support of VISOR for data sharing. Finally, we thank the Mastcam-Z instrument team for use of the caltarget witness samples.

Data Availability Statement

TANAGER’s computer-aided design (CAD), electrical schematics, and bill of materials (BOM) are publicly available as Hoza et al. (2023). TANAGER’s custom software (“tanager-feeder”), which commands its motors, interfaces with the spectrometer, and visualizes the data, is open-source and available as Hoza (2023). All spectral data acquired for TANAGER’s validation and characterization are available as Lapo et al. (2024).

References


J.F. Bell III, A. Godber, S. McNair, M.C. Caplinger, J.N. Maki, M.T. Lemmon, et al., The Mars Science Laboratory Curiosity rover Mast Camera (Mastcam) instruments: pre-


Shaw, A., Daly, M. G., Cloutis, E., Basic, G., Hamilton, D., Tait, K., et al. (2016). Reflectance properties of grey-scale Spectralon® as a function of viewing angle,


TANAGER: Design and Validation of an Automated Spectrogoniometer for Bidirectional Reflectance Studies of Natural Rock Surfaces

Melissa Rice, Kristiana Lapo, Kathleen Hoza, Ed Cloutis, Mike Kraft, Sean Mulcahy, Dan Applin

Abstract

Laboratory measurements of reflectance spectra of rocks and minerals at multiple viewing geometries are important for interpreting spacecraft data of planetary surfaces. However, efficiently acquiring such measurements is challenging, as it requires a custom goniometer that can accommodate multiple, bulky samples beneath a movable light source and detector. Most spectrogoniometric laboratory work to date has focused on mineral mixtures and particulates, yet it is also critical to characterize natural rock surfaces to understand the influence of texture and alteration. We designed the Three-Axis N-sample Automated Goniometer for Evaluating Reflectance (TANAGER) specifically to rapidly acquire spectra of natural rock surfaces across the full scattering hemisphere. TANAGER has its light source and the spectrometer’s fiber optic mounted on motorized rotating and tilting arcs, with a rotating azimuth stage and six-position sample tray, all of which are fully motorized and integrated with a Malvern PanAnalytical ASD FieldSpec4 Hi-Res reflectance spectrometer. Using well-characterized color calibration targets, we have validated the accuracy and repeatability of TANAGER spectra. We also confirm that the system introduces no discernable noise or artifacts. All design schematics and control software for TANAGER are open-source and available for use and modification by the larger scientific community.
1. Introduction

Studying the composition and distribution of minerals on planetary bodies is critical to understanding their surface evolution. Across the solar system, key mineral identifications have been made using visible to near-infrared (VNIR) spectrometers on ground- and space-based telescopes, orbital spacecraft, and landers. VNIR reflectance spectroscopy relies on the analysis of diagnostic absorption features, specifically their band center wavelength positions, shapes, and depths (e.g., Bishop et al., 2020). However, VNIR reflectance spectra are not influenced by mineral composition alone. Variables such as grain morphology (size and shape), temperature, and nonlinear mixing effects also influence the shapes, positions and depths of diagnostic absorption features (e.g., Clark & Roush, 1984; Clark et al., 1999).

In particular, viewing geometry (photometric) effects can complicate remote sensing interpretations. Conversely, once understood, photometric effects can allow for richer inferences to be drawn than would otherwise be possible. For example, photometry has been used to constrain the microtexture of surface materials including roughness and porosity (e.g., Bandfield et al., 2015; Hapke and Sato, 2016; Shepard et al., 2017). Microtextural characteristics can in turn be used to understand surface processes (e.g., regolith/soil formation and evolution), to serve as inputs to planetary thermal models, and to constrain mechanical properties relevant to exploration. Such investigations have been performed for the Moon (e.g., Shkuratov et al., 1999), asteroids (e.g., Clark et al., 2002), Mars (e.g., Johnson et al., 1999; see also Fernando et al., 2015; Johnson et al., 2006a-b; Johnson et al., 2021, 2022; Lichtenberg et al., 2007) and other planets (e.g., Veverka et al., 1988; Schröder & Keller, 2009). Furthermore, several models have been developed to better understand how the microscale physical properties of surfaces influence photometry (e.g., Hapke, 1993; Shkuratov et al., 1999).
Photometric effects, however, are often not included in laboratory VNIR reflectance measurements of reference rocks and minerals. Many commercial VNIR spectrometers do not allow users to easily control the incidence and emission angles, and most laboratory spectra are acquired with a single, fixed geometry (e.g., incidence = 30°, emission = 0°). In contrast, telescopic and spacecraft observations of planetary surfaces are acquired at a variety of geometries, depending on the relative positions of the light source (Sun), target material (planetary surface), and detector (spectrometer/camera) (e.g., Figure 1). Custom-built goniometers (which control the orientations of the incidence light and spectrometer’s detector) are required, therefore, for reproducing photometric effects in the laboratory.

Figure 1. Cartoon of viewing geometries relevant to spacecraft exploration of planetary surfaces, for the specific example of spectroscopy measurements by a rover on Mars. Geometries shown include emission angle $e$, incidence angle $i$, and azimuth angle $\phi$. Phase angle $g$ is the angle between $e$ and $i$.

To date, such “spectrogoniometry” measurements have focused primarily on particulate samples of uniform grain size and composition (e.g., Pommerol et al., 2013; Shephard and
Helfenstein, 2007) or two-phase mixtures (e.g., Pilorget et al., 2016; Stack & Milliken, 2015). A limited number of laboratory studies have acquired spectrogoniometric measurements for whole rocks (Guinness et al., 1997; Shepherd & Arvidson, 1999). However, the compounding effects of composition, alteration, microtexture, and viewing geometry on complex rock surfaces are still poorly understood. Working with natural rock surfaces in the laboratory poses several challenges. For example, bulky samples require a non-standard goniometer setup with an adjustable sample stage and large incidence and emission arms.

We have designed and built such a system for the Mars Lab at Western Washington University (WWU) in order to characterize the spectrogoniometry of a variety of rock and mineral samples. Specifically, WWU’s Mars Lab studies VNIR reflectance spectra of naturally-weathered rocks as analogs to the geologic materials encountered by the Mars Exploration Rovers (MERs), the Mars Science Laboratory (MSL) Curiosity rover, the Mars-2020 Perseverance rover, and future landed missions. The science needs of the Mars Lab necessitate rapid acquisition of spectra from large numbers of bulky samples. For efficiency in collecting large datasets at high angular resolution, it is important to use a motorized system for precise, repeatable positioning of the light source, detector, and sample. Furthermore, software is required to automate the goniometer and allow it to interface with the spectrometer collecting the data. While some aspects of this ideal system have been developed previously for other laboratories (e.g., Biliouris et al., 2007; Camon & Lemelin, 2024; Painter et al., 2003; Pilorget et al., 2016; Pontin et al., 2018; Shepard and Helfenstein, 2007), no fully-automated system (to our knowledge) exists for goniometry with a hyperspectral instrument for measuring a variety of whole rock samples.
Here, we describe WWU’s Three-Axis N-sample Automated Goniometer for Evaluating Reflectance (TANAGER). (The acronym TANAGER also has local significance, as the Western Tanager is a brightly colored bird native to Washington state.) TANAGER derives heritage from the WWU Mars Lab’s previous planar goniometer (Hoza & Rice, 2019), which allows for automated collection of spectra from multiple bulky samples at varying incidence and emission angles. TANAGER substantially improves upon the planar goniometer design with the capability to collect out-of-plane geometries (i.e., varying azimuth), which is necessary to characterize the full bidirectional reflectance distribution function (BRDF). In partnership with the Seattle-based engineering company First Mode, LLC, we designed and characterized TANAGER to support rapid and comprehensive spectrogoniometric studies of natural rock samples.

2. Performance Requirements

To enable rapid collection of reflectance spectra from multiple rock surface across the full scattering hemisphere – as well as rapid analysis of the spectrophotometric datasets – we defined the following top-level requirements for TANAGER:

1. **Scientific Purpose:** The system shall enable collection of VNIR spectra at a range of geometries relevant to spacecraft measurements.

2. **Sample Type:** The system shall enable measurement of bidirectional reflectance for natural, unprocessed samples.

3. **Time Efficiency:** The system shall enable the following 2 concepts of operations: “Quick Runs” (8 hour time limit), and “Detailed Runs” (168 hour time limit).

4. **Data Visualization:** The system shall provide a means of documenting and visualizing the collected spectra.
5. **Safety**: Use of the system shall not result in damage to people, the goniometer, or other equipment, facilities, or samples.

To meet these requirements, TANAGER’s high-level design (Figures 2-3) differs substantially from other spectrogoniometer systems, as we outline in Section 3.

![Schematic of TANAGER with major components labeled. For scale, the dimensions of the baseplate are 80 x 95 cm.](image)

**Figure 2.** Schematic of TANAGER with major components labeled. For scale, the dimensions of the baseplate are 80 x 95 cm.
Each top-level requirement yields multiple sub-requirements (Table 1). First Mode, LLC evaluated all requirements except for sub-requirements 1.13, 2.1, 2.2 and 2.4, which were evaluated at WWU upon delivery of TANAGER in Spring 2021 (see Text S1-S5). Every sub-requirement has been met except for the detector head not falling inside the incident light beam for \( g \geq 20^\circ \) (sub-requirement 1.1). However, we find the small shadow cast at \( g = 20^\circ \) to be acceptable, as it is outside the detector pointing (Figure S1). Eight of the sub-requirements were also reevaluated after 300 hours of TANAGER run time (Table S1), which yielded recommendations for long-term operations of the hardware (Table S6).

**Table 1:** Summary of the sub-requirements for TANAGER, which derive from the top-level requirements listed in the text. All sub-requirements have been met except for 1.10 (which was met within an acceptable threshold, as discussed in the text).

<table>
<thead>
<tr>
<th>Sub-Requirement</th>
<th>Description</th>
</tr>
</thead>
</table>
| 1.1 Range                | The system shall enable measurements with  
  ● azimuth from 0° to 170°  
  ● emission from -70° to 70°  
  ● incidence from -70° to 70°                                                                 |
<p>| 1.2 Phase angle          | The system shall enable measurements at phase angles from 10° to 140°                                                                         |
| 1.3 Angular control      | The system shall have knowledge and control of detector and light source with 1° steps in all directions                                      |
| 1.5 Pointing accuracy - light source | The center of the illuminated spot shall not deviate from the target point by more than +/- 10% of the illuminated spot diameter |
| 1.6 Pointing accuracy - detector | The center of the detector spot shall not deviate from the target point by more than +/- 10% of the detector spot diameter |
| 1.7 Light bulb operating lifetime | The light bulb shall have an operating lifetime of at least 100 hours                                                                   |
| 1.8 Target plane indicator | The goniometer shall provide the user with a clear indicator of whether a surface is in the target plane                                      |</p>
<table>
<thead>
<tr>
<th>Requirement</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.9 Proximity to light source</td>
<td>The detector head and fiber optic shall not come within 5 mm of the light source during normal operations</td>
</tr>
<tr>
<td>1.10 No incident light on detector</td>
<td>The detector head shall not be inside the incident light beam for $g \geq 20^\circ$</td>
</tr>
<tr>
<td>1.11 Signal drift from heating at small phase angles</td>
<td>At geometries with phase angles below $20^\circ$, the standard deviation for repeated measurements taken over the course of 4 minutes shall not be greater than 0.02</td>
</tr>
</tbody>
</table>
| 1.12 Noise | For both light and dark samples, noise measured against a Savitzky-Golay smoothed spectrum with window size = 19, order = 2 shall not exceed:
   - +/- .001 in mid-range (500-2400 nm) wavelengths
   - +/- .005 for long (2400-2500 nm) and short (450-500 nm) wavelengths |
| 1.13 Polarization artifacts | Polarization artifacts shall not be more than 0.1 for basalt (or a similar sample) at any geometry where azimuth = 180° or 0° |
| 2.1 Detector spot size | The detector spot size on the sample shall have a diameter less than the size of the Spectralon puck at $e = 70^\circ$ (9.1 cm) |
| 2.2 Light spot size | The brightest part of the light spot size shall be 0.5 cm to 3 cm in diameter at $i = 0^\circ$ |
| 2.3 Sample tray repeatability | Each of the 6 sample tray positions shall be repeatable to within +/- 1 mm |
| 2.4 Sample tray vibration | Sample tray movements and vibrations from other actuators shall not disturb the positioning of rounded coarse sand grains in sample cups |
| 2.5 Sample accommodation | The sample tray shall accommodate up to 5 cylindrical samples (9.1 cm diameter, 0 to 5.1 cm height) plus 1 Spectralon puck |
| 2.6 Center-of-sample markings | The sample tray shall have marked center of sample points for each position |
| 2.7 Large sample compatibility | The sample tray shall not interfere with the measurement of spectra for large (>10 cm) samples |
| 2.8 Irregular sample positioning | The sample tray shall enable 5 different wedge-shaped samples plus the Spectralon puck to be positioned each with a surface that is:
   - In the target plane to within +/- 1 mm
   - Parallel with the target plane to within +/- 5°
   - Sample heights may range from 0-5 cm, diameters from 3-9 cm |
<p>| 3.1 Viewing Geometries | Actuators shall be capable of positioning incidence, emission, and azimuth as described in sub-requirement 1.1 |
| 3.2 Sample tray rotation speed | Sample tray movements shall occur at an average speed of at least $4^\circ$ per second |
| 3.3 Viewing geometry adjustment speed | Incidence, emission, and azimuth movements shall occur at an average speed of at least $0.2^\circ$ per second |</p>
<table>
<thead>
<tr>
<th>Specification</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>3.4 Automatic software startup</td>
<td>Software on the spectrometer computer and raspberry pi shall start automatically</td>
</tr>
<tr>
<td>3.5 Legacy software</td>
<td>Unless otherwise noted, software shall provide the same functionalities and experience as existing software</td>
</tr>
<tr>
<td>3.6 Iteration across a range</td>
<td>Software shall enable data collection while iterating at a set interval through a range of incidence, emission, and azimuth angles as described in subrequirement 1.1</td>
</tr>
<tr>
<td>3.7 Goniometer visualization</td>
<td>Software shall provide a visualization showing the software's understanding of the current state of the 3D goniometer including incidence angle, emission angle, azimuth angle, and sample tray position</td>
</tr>
<tr>
<td>3.8 Communication speed (microcontroller)</td>
<td>Communicating commands to and from the microcontroller shall take no longer than 1 second</td>
</tr>
<tr>
<td>3.9 Communication speed (spectrometer computer)</td>
<td>Communicating commands to and from the spectrometer computer shall take no longer than 1 second</td>
</tr>
<tr>
<td>3.10 Time limit (limited run)</td>
<td>A limited run of data collection shall take no longer than 8 hours</td>
</tr>
<tr>
<td>3.11 Number of samples (limited run)</td>
<td>A limited run of data collection shall characterize 1 sample</td>
</tr>
</tbody>
</table>
| 3.12 Viewing geometries (limited run) | A limited run of data collection shall include the following geometries:  
  ● For a single plane (az = 0°) measure e, i with 10° resolution  
  ● Outside that plane - 30° azimuthal resolution, 5 geometries at each azimuth  
  ● Leave out reciprocal and rotationally equivalent geometries |
| 3.13 Time limit (detailed run) | A detailed run of data collection shall take no longer than 168 hours |
| 3.14 Number of samples (detailed run) | A detailed run of data collection shall characterize 5 samples |
| 3.15 Viewing geometries (detailed run) | A detailed run of data collection shall include the following geometries:  
  ● 30° azimuthal resolution  
  ● At each azimuth, 10° angular resolution for incidence, emission |
<p>| 3.16 Spectra per sample | At each geometry, a measurement of a single sample shall consist of averaging 200 spectra |
| 3.17 Human operator time | Setting up a run of data collection shall not require more than 60 minutes of time from a human operator |
| 4.1 Data processing/visualization | Software shall be capable of processing and plotting data sets of up to 5000 spectra |
| 4.2 Feature requests | Additional features may be added |
| 5.1 Light source casing temperature | The temperature of the light source shall not exceed 60° C |</p>
<table>
<thead>
<tr>
<th>5.2 Securability</th>
<th>The sample tray shall be securable</th>
</tr>
</thead>
<tbody>
<tr>
<td>5.3 Position detection</td>
<td>The goniometer incidence, azimuth, and emission positions and the sample tray position shall be detected at the start of operations</td>
</tr>
<tr>
<td>5.4 Collision avoidance</td>
<td>Software shall not allow incidence, emission, or azimuth arms to collide with each other</td>
</tr>
</tbody>
</table>

### 3. Design and Characterization

#### 3.1 Incidence Arm and Light Source

The primary design difference between TANAGER and most existing goniometers is the use of rotating and tilting arcs instead of straight arms, with the addition of cylindrical bronze ~1.5 kg counterbalance weights to provide stability and require less torque from the motors (Figure 4). The TANAGER system enables incidence and emission angles of -70° to 70°, and stepper motors allow for automated, repeatable movements to defined geometries sampling the full scattering hemisphere. This range of angles is sufficient to characterize scattering behavior using the Hapke model (e.g., Schmidt and Fernando, 2015).

Using two green laser guides on the incidence arm (Figure 5), we can ensure that the surfaces of bulky samples are positioned precisely in the focal plane. The brightest portion of the illuminated spot size in the focal plane at i = 0° is 2.7 cm in diameter, and larger at higher incidence angles (but always <9.1 cm, per sub-requirement 2.2; Table 1). Because the illuminated spot size is not actively controlled, it is possible to measure slightly different portions of the sample surface at different incidence angles, especially with high emission angles where the detector spot (which is similarly not actively controlled) can be larger than the
illuminated spot. Users should take this into consideration for high phase angle measurements of non-uniform samples.

![Schematic of TANAGER’s incidence arm. The diameter of the arc is 67 cm.](image)

**Figure 4.** Schematic of TANAGER’s incidence arm. The diameter of the arc is 67 cm. Illumination is provided by a Thorlabs VNIR light source, and two bronze weights provide counterbalance. Two green laser guides intersect at the focal plane.

![Green laser guides indicate when the sample is out of the focal plane (left) and within the focal plane (right, when two dots become one).](image)

**Figure 5.** Green laser guides indicate when the sample is out of the focal plane (left) and within the focal plane (right, when two dots become one).

The apex of the incidence arm supports a Thorlabs SLS201L light source with integrated cooling system and peak output near 1000 nm (Figure 6). This commercial light was selected for its relatively long bulb lifetime, sufficient power output across the 400-2500 nm wavelength range, and minimal heating. We characterized heating on color standards and geologic targets in the focal plane (Text S1) and found the temperature increases to be minimal: Spectralon®, which
heated negligibly (0.4°C), and other targets’ temperatures increased by 2-4°C over typical
exposure durations (~2 minutes of direct illumination during nominal TANAGER operations)
(Figure S2). We also characterized the effects of incident light heating on adsorbed water by
monitoring spectral changes to powdered anhydrite (CaSO₄) over time (Text S2). During 30
minute periods of exposure, we observed no changes to the hydration absorptions attributed to
adsorbed water on grain surfaces (Figures S2-S4), which gives us confidence that the sample
heating is too minimal to drive adsorbed water off mineral grains or otherwise dehydrate
samples.

![Thorlabs VNIR light source with power distribution curve](image)

**Figure 6.** Thorlabs VNIR light source (left) with power distribution curve for a blackbody and as measured (right).

### 3.2 Emission Arm

TANAGER interfaces with a Malvern PanAnalytical ASD FieldSpec4 Hi-Res reflectance
spectrometer (hereafter, “FieldSpec”; Section 3.5), and its emission arm is designed to
accommodate the fiber optic cable attached to the spectrometer (the reflectance probe). Like the
incidence arm, the emission arm uses stepper motors for precise, repeatable positioning of
emission angles from -70° to 70°. The design of the arm is an arc (Figure 7) with a collimating
lens that reduces the detector spot size at the focal point. Reflected light entering the collimator is directed to the fiber optic cable via an angled mirror at the end of the emission arm. We characterized how the detector spot size changes with emission angle (Text S3) and found a minimum of 1.6 cm at $e = 0^\circ$ and a maximum of 3.5 cm at $e = 70^\circ$ (Table 2). At small incidence angles, this means that the detector spot falls entirely within the illuminated portion of the sample for emission angles < 50°.

![Fixed section](Image)

**Fixed section**

![Joint](Image)

**Joint**

![Rotating section](Image)

**Rotating section**

**Figure 7:** Components of the emission arm’s tubing, which guides the position of the FieldSpec’s fiber optic cable and maintains a wide arc at all geometries.

**Table 2:** Detector spot size ranges measured for different emission angles (see Text S1).

<table>
<thead>
<tr>
<th>Emission angle ($^\circ$)</th>
<th>Measured Spot Size Range (cm)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>1.6-2.0</td>
</tr>
<tr>
<td>15</td>
<td>1.8-2.6</td>
</tr>
<tr>
<td>30</td>
<td>1.8-2.2</td>
</tr>
<tr>
<td>50</td>
<td>2.4-2.8</td>
</tr>
<tr>
<td>70</td>
<td>2.8-3.5</td>
</tr>
</tbody>
</table>
The emission arm design ensures that the spectrometer’s fiber optic cable (the reflectance probe) does not bend in any geometry. A guide tube keeps the fiber in a repeatable position from one measurement to the next, which consists of a short, fixed portion close to the detector tip and a longer, rotating portion farther back (Figure 7). This tubing allows for the fiber optic to be easily removed and replaced when the FieldSpec needs to be detached from TANAGER (e.g., when used with a Malvern Panalytical Contact Probe or Small Diameter Probe). To prevent bending of the fiber optic, the system is designed to maintain a 35 cm diameter of curvature.

3.3 Azimuth Turntable

The incidence arm is mounted to a geared turntable which controls azimuth angle between 0° and 180° (Figure 8). The large gear ratio reduces the necessary torque and increases angular accuracy. The system includes a homing routine with stops installed onto the baseplate. One challenge in the azimuth design is the need to manage cables for the light source, incidence motor, and incidence encoder as azimuth changes. The solution in TANAGER’s initial design used the combination of slider, coiled cable, and spring-loaded arm to enable consistent motion across the azimuth range (Figure 9). However, upon extensive use in WWU’s Mars Lab, we found that the slider’s and spring arm’s motions were finicky, so we attached the coiled cable to a fixed lab surface with ample clearance instead (Figure 10).
**Figure 8.** Left: Schematic of the azimuth turntable mounted with the attachments and stepper motor for the incidence arm. Middle: Detail of gears for the azimuth turntable. Right: Schematic of the homing mechanism on the azimuth baseplate.

**Figure 9.** Initial cable management solution for the full range of azimuths (0° to 180°).
Figure 10. Final cable management solution for the full range of azimuths (0° to 180°).

3.3 Sample Trays

The goniometer design includes two stages for positioning samples within the focal plane. Both are motorized and can rotate up to five samples in and out of the field of view with a Spectralon® white reference correction at each geometry. The first is a single, height-adjustable surface designed for multiple samples of the same height (e.g., particulates in sample cups) or for a single, bulky hand sample (Figure 11). For use with this stage, we designed sample cups at the
same height as the white reference and risers for positioning Scanning Electron Microscope (SEM) mounted samples.

Figure 11. Left: Single-height, rotating sample stage. Right: Custom sample cups and risers for SEM mounts designed with the same height as the Spectralon® white reference puck.

The other stage consists of six pie-slice-shaped sample supports, each of which can be moved independently (height and tilt) to accommodate a variety of bulky samples (Figure 12). Many degrees of freedom are required for positioning a near-flat portion of each sample into the focal plane. Adjustable screws can be added/removed to keep samples in place, and multiple sample supports can be used to support a single, awkward sample (Figure 12 right). In characterizations of sample tray motion during TANAGER operations (Text S4), we found that vibration was undetectable during incidence and emission arm motions, and minimal during azimuth and tray motions (Figure S5). TANAGER’s movements are highly unlikely to change the positions of samples on the tray or shift loose material within sample cups (Figure S6).
Figure 12. Left: Schematic of the multi-height, rotating sample stage. Six independently-adjustable, pie-slice-shaped supports allow for the positioning of a variety of samples. Right: Example of a bulky, awkward sample positioned with a horizontal surface in the focal plane using two supports and stabilizer screws.

3.4 Paint

Before delivery of TANAGER, all components were coated with a matte black paint to minimize stray light reflections from the metallic surfaces. We collected VNIR spectra for a range of different black paint options (LabIR Paints, Rustoleum, Fusion, black30), and all exhibited similar spectral shapes and low albedos throughout the 400-2500 nm range. Specular properties for all materials were also similar. Thus, we looked to mechanical adhesion and wear and selected LabIR Paints (https://paints.labir.cz/en/) because it performed best in mechanical tests. We applied the black paint to TANAGER via aerosol (Figure 3).
3.5 Spectrometer Interface

Sample spectra (averages of 200 for each) are measured relative to a Spectralon® white reference target at each geometry and corrected for minor (<2%) irregularities in absolute reflectance and for small offsets at 1000 and 1830 nm where detector changeovers occur (e.g., Cloutis et al., 2008). The ideal white reference material would be a perfectly Lambertian reflector (scattering incident light equally at all viewing geometries); in practice, however, such a material does not exist, but the geometry-dependent reflectance properties of Spectralon® have been well-documented (e.g., Shaw et al., 2016). We have incorporated the published Spectralon® corrections for high phase angles from Bhandari et al. (2012), using a linear interpolation when needed, into the analysis software (Section 2.9).

Other challenges to the spectrometer interface occur at high phase angles, where the emergence of artifacts near 1100 and 1310 nm in spectra from FieldSpec and similar spectrometers have been documented (e.g., Buz et al., 2019) and shown to originate from polarization of the sample and probe (Levesque & Dissanska, 2016). These polarization artifacts are challenging to correct, but fortunately, their wavelength positions do not interfere with the locations of the prominent spectral features and absorptions in rock-forming minerals and their alteration products. We quantified the strength of these artifacts for our prototype planar goniometer (Hoza & Rice, 2019), for a variety of materials at a range of phase angles, and found that they were consistently negligible (<1%) at phase angles between $g = -20^\circ$ and $g = 40^\circ$. Therefore, we designed an option to omit the region 1050-1350 nm from TANAGER’s high phase angle analyses, as done by Buz et al. (2019). However, we have rarely needed this option.
in practice, as TANAGER’s spectra rarely exhibit polarization artifacts (and, when they do appear, they are < 2%; Text S5; Figure S7).

3.6 Automation and Control Software

Automation is a critical design component of TANAGER. Our previous studies verified the need for an automated system: using our prototype planar goniometer (Hoza & Rice, 2019) with a simple control software, we found that our rate of data collection increased by almost an order of magnitude. When manually positioning targets and the goniometer arms, acquiring measurements at 10 viewing geometries with Spectralon® white reference correction took roughly 90 minutes for a single sample and required an attendant in the lab to adjust the goniometer and perform the white reference calibration every few minutes. However, with automation, we acquired spectra of five samples with white reference corrections at 10 viewing geometries each in under 60 minutes total, including time for data processing and plotting, with minimal need for supervision by a lab attendant (Hoza & Rice, 2019). For more detailed analyses requiring high angular resolution (~100 geometries), automation reduced the total acquisition time per sample from ~15 to ~2 hours.

For TANAGER, a total of four stepper motors drive the incidence, emission, azimuth, and sample tray components, as described above. First Mode, LLC designed custom software for TANAGER in open source packages called “tanager-feeder” (Hoza, 2023). The software operates three computers all connected to a local spectroscopy lab network (Figure 13):

1. **Control computer.** This is where the user gives input. Software running on this computer includes a Python Graphical User Interface (GUI) that allows the user to input all parameters relating to sample configuration, spectrometer configuration, and desired
viewing geometries. This GUI also displays information about the current state of the system (Figure 14) and includes a log of all actions taken during the current session.

2. **Spectrometer computer.** This computer is controlled via command files generated by the control computer and dropped into a shared folder on the local network. Following instructions in these command files, it runs GUI automation software that operates the proprietary spectrometer control software (RS3) and spectral processing software (ViewSpec Pro). This enables the instrument to be optimized and for a white reference taken at each viewing geometry. After each run of data collection, this spectral processing software is used to apply a splice correction to remove artifacts generated at the positions where spectrometer detectors overlap.

3. **Raspberry Pi.** This computer is also controlled via command files generated by the control computer and dropped into a shared folder on the local network. Following instructions in these command files, it operates the motors driving the goniometer arms and sample tray. The software is designed with safety in mind; for example, it keeps the emission and incidence arms out of harm’s way while other parts are rotating. The control system also notices if motorized parts are not making progress and stops and alerts the user via the control computer.
Figure 13. Panoramic photo of the lab containing TANAGER (upper left) showing the relative placements of the FieldSpec, Raspberry Pi, control laptop, and spectrometer computer. Blackout curtains are hung behind TANAGER in order to minimize stray light.

Figure 14. Screenshot of “tanager-feeder” control software GUI with settings on the left, visualization of current goniometer and sample stage configuration on the upper right, and command line interface at lower right.

3.7 Analysis Software

In addition to operating the goniometer and spectrometer, the “tanager-feeder” software includes a suite of tools that can be used to view and analyze spectrophotometric data. In the
simplest case, a selected set of spectra are plotted with wavelength on the x-axis in nanometers and reflectance (relative or absolute) on the y-axis (Figure 15a). Additional analytical capabilities include normalizing spectra to 1.0 at a given wavelength (Figure 15b); calculating spectral slope (defined as the change in relative reflectance divided by the change in wavelength in nm; Figure 16); calculating band centers and depths of features between user-defined shoulder wavelength positions (as defined by Clark, 1999); calculating average reflectance for all values between a give wavelength range; adding offset values to spectra for clarity (Figure 17); and excluding wavelength regions with known artifacts (Figure 18).

Figure 15: Example of spectra before (a) and after (b) normalization to 1.0 at wavelength 680 nm.
**Figure 16:** Spectral slopes are calculated from a range of wavelengths identified for spectra of interest (a) and can be plotted as a function of phase angle $\phi$ (b). In this case, slopes are calculated from 550-950 nm and are shown to become less negative as phase angle increases.

**Figure 17:** Overlapping spectra (a) can be hard to interpret, but adding offsets to samples can add clarity (b).

**Figure 18:** Polarization artifacts can appear within wavelengths 1000-1400 nm at high phase angles (a), so these regions can be omitted from our results for given geometries and replaced with dashed lines (b). Spectra shown are from the WWU Mars Lab’s planar goniometer (Hoza & Rice, 2019); in practice, TANAGER spectra rarely exhibit polarization artifacts (Text S5; Figure S7).

When interpreting spectra taken at a wide range of geometries, alternative visualization techniques can be beneficial for displaying some photometric behaviors. For example, to show the shapes of scattering lobes for measurements in a single plane (fixed azimuth), two-dimensional hemispherical plots can be much more effective than the original spectra (Figure
19). Our software also allows fixed azimuth data to be displayed with a heatmap; in these plots, emission angle is on the x-axis, incidence angle on the y-axis, and a user-defined parameter (such as reflectance at a given wavelength, band depth of a specific features, etc.) is represented by a color scale (Figure 20). For three-dimensional datasets (including variations in azimuth angle), the software enables visualizations of spectrophotometric behaviors as scattering lobes and/or heatmaps (Figure 21).

**Figure 19:** Examples of two-dimensional hemispherical plots: (a) Reflectance is measured for three samples at an incidence angle of -20 degrees and emission angles varying from 0 degrees to 60 degrees. (b) Reflectance values at 680 nm are plotted on a hemispherical plot with reflectance on the radial axis and emission angle varying with theta. Spectra shown are of uncoated (blue, green) and silica-coated (red) basalt surfaces (Hoza, 2019).
Figure 20: Examples of two dimensional “heat map” plots: (a) Reflectance is measured at all viewing geometries for a given sample (incidence = $-50^\circ$ shown here). (b) Reflectance at 680 nm is plotted as a heat map in incidence, emission space with a color scale representing a range of reflectance. (c) For a different sample, slope from 550-950 nm is measured for normalized spectra at all viewing geometries (incidence = $-50^\circ$ displayed here). (d) Slope is then plotted on a heat map over incidence, emission space with the color scale corresponding to different slopes.
Figure 21: Examples of three-dimensional hemispherical plots of scattering patterns for the Spectralon® white reference (which is non-Lambertian above i = 45°), for reflectance values at 680 nm.

3.8 Operational Procedures

Approximately one hour of human operation time is required before TANAGER data collection can be initiated. A number of startup procedures are required to place and secure samples, perform safety checks, input run parameters, and generally ensure that data are collected safely and effectively. Below, we provide a high-level description of human-operator startup tasks for TANAGER data collection in “automatic mode”: 
1. **FieldSpec warmup:** Turn on the FieldSpec spectrometer to allow it to warm up for 60 minutes, as recommended by the manufacturer (ASD Inc., 2017).

2. **Sample positioning (initial):** While the FieldSpec is warming up, perform the initial sample placements on the sample stage, level targets using a bubble level, and adjust the targets into the measurement plane with the indicator lasers (Figure 5). For larger, natural, or irregular samples, this may require significant manipulation of the sample tray stage and/or securing the sample with supports and stabilizer screws (Figure 12). Finally, test for collisions by manually moving the emission arm to +/- 50° (the steepest emission angle during sample tray rotation), rotating the sample tray 360°, and readjusting sample placement as necessary.

3. **Software setup:** After initial sample placement, turn on the Raspberry Pi, control computer, and spectrometer computer. In the user interface on the control laptop, configure the control computer interface to match the physical TANAGER set up, set the number of spectra to be collected, select the correct white reference calibration file, enter the desired geometries, and name the samples.

4. **Sample positioning (secondary):** With Raspberry Pi on and the stepper motors engaged, recheck the sample placement, leveling, height, and collision risk for each sample and make final adjustments as necessary.

5. **Data collection:** During data collection, light sources unrelated to data collection (e.g. overhead lights and unnecessary computer monitors) should be turned off. A human operator may either remain in the lab (e.g. for a short run of 30 minutes) or leave the lab for the duration of the run (e.g. for multi-day runs) in order to
eliminate stray light from outside the lab. Western Mars Lab uses an infrared webcam to monitor the control computer software and TANAGER hardware for run completion or unexpected errors when the human operator is not in the lab.

4. Data Validation

4.1 Cross-Calibration

We validated TANAGER’s data quality by reproducing measurements of calibration target (“caltarget”) materials from Buz et al. (2019). The caltargets are a set of exceptionally well characterized color standards and are the reference targets for the Mastcam-Z instrument on the NASA Mars 2020 Perseverance rover (Kinch et al., 2020). These caltargets have also been used in the calibration of Mastcam-Z’s legacy instruments: Mastcam on the NASA Mars Science Laboratory Curiosity rover (Bell et al., 2017) and Pancam on the NASA Mars Exploration Rovers (Bell et al., 2006). The eight caltargets include AluWhite from Avian Technologies LLC; and Cyan, Green, Red, Yellow, Gray33, Gray70, and Black from Lucidion Inc.. Spectra from each target were collected at same geometries of Buz et al. (2019) and evaluated at subset of phase angles: backscattering geometry (i = 30°, e = 45°, az = 0°, g = 15°), standard geometry (i = 0°, e = 30°, az = 0°, g = 30°), specular geometry (i = -30°, e = 30°, az = 0°, g = 60°), forward scattering geometry (i = -45°, e = 30°, az = 0°, g = 75°), and very forward scattering geometry (i = -70°, e = 58°, az = 0°, g = 128°). Relative root mean square error (RMSE, defined in Text S3) was calculated to compare datasets. We consider a relative RMSE of 5% or less to be an acceptable threshold of error (as is the case in the radiometric calibration of flight hardware such as Mastcam-Z; Hayes et al., 2021).
Spectra from TANAGER agree with those from Buz et al. (2019) to within 0.05 reflectance units for the color and black standards, and to within 0.01 for the grayscale standards, in all geometries except for the highest phase angles (Figures 22-23 and Figures S8-S9). Wavelengths near 1100 nm and 1300 nm typically have large residuals (e.g., Figure 23 gray), which we attribute to known polarization artifacts that are prominent in the data from Buz et al. but nearly absent in TANAGER spectra (see Text S5). We also observe structure in the residuals near 1900 nm (e.g., Figure 22), where there is an H$_2$O absorption; Buz et al. (2019) note variations in this band strength in their spectra which they attribute to water in the instrument path length, and they recommend caution when interpreting small fluctuations in this region.

We observe the same general scattering behaviors for all targets as those reported by Buz et al. (2019): the brighter samples (light gray, red, cyan and yellow) are quasi-isotropic, the AluWhite sample is weakly backward scattering, and the darker samples (black, dark gray and green) are strongly forward-scattering. TANAGER spectra of the brighter samples suggest they are more isotropic than demonstrated by Buz et al. (2019) (i.e., TANAGER spectra show less variation in reflectance at high phase angles; Figure 22, Figure S8). The two highly forward-scattering geometries ($i = 30^\circ$ and $e = -58^\circ, -70^\circ$) show reversed behavior in TANAGER spectra compared to Buz et al. (2019); however, the TANAGER spectra are more consistent with the known scattering behaviors for these targets (e.g., the $e = -70^\circ$ spectrum is higher reflectance than the $e = -58^\circ$ spectrum for strongly forward-scattering targets; Figure 23, Figure S9). Therefore, the discrepancies between the two labs’ datasets may indicate improvements in TANAGER spectra over the previously-published versions.
Figure 22: Spectra of the cyan and red Mastcam-Z caltarget witness samples at multiple viewing geometries from TANAGER (top) compared to Buz et al. (2019) (middle), with residuals (bottom). All measurements were acquired at $i = 30^\circ$ and $az = 0^\circ$. 
Figure 23: Spectra of the light gray (70% white) and black Mastcam-Z caltarget witness samples at multiple viewing geometries from TANAGER (top) compared to Buz et al. (2019) (middle), with residuals (bottom). All measurements were acquired at $i = 30^\circ$ and $az = 0^\circ$. 
To minimize differences in absolute reflectance and focus on differences in spectral shape, we also normalized spectra to 1.0 at 754 nm and calculated relative RMSE at a representative range of geometries. The normalized spectra (Figure 24) have only minor differences in spectral shape and slope (except for the light gray target at \( g = 128^\circ \)). Relative RMSE values (Table 3) are less than 5% with two exceptions: (1) the black target and (2) highly forward-scattering geometries. We attribute the black target’s high relative RMSE to its dark albedo and low signal-to-noise, so we do not find these values concerning, but recommend caution when interpreting subtle spectral shapes in TANAGER spectra of dark materials.

The high relative RMSE values for the very forward-scattering geometry (\( g = 128^\circ \)) may result from differences between the Buz et al. (2019) and TANAGER lab setups. At the highest measurable phase angles, it is possible that TANATER’s detector may receive stray light reflected from lab walls and cabinets at high emission angles. To test and potentially mitigate scattered light effects, we hung blackout curtains on the surfaces immediately adjacent to TANAGER (shown in Figure 13) and recollected the \( g = 128^\circ \) spectra, which led to general decreases in overall reflectance (Figure S10) and improvements in relative RMSE values (Table 3). We now hang black curtains over all surfaces adjacent to TANAGER as part of our standard procedure.
Figure 24: Spectra normalized to 754 nm of select caltargets from TANAGER (darker lines) and Buz et al. (2019) (lighter lines) at a range of viewing geometries. Minor artifact peaks are marked in the Gray70 and Black Buz et al. (2019) spectra for $g = 75^\circ$ and $g = 128^\circ$.

<table>
<thead>
<tr>
<th></th>
<th>$g = 15^\circ$</th>
<th>$g = 30^\circ$</th>
<th>$g = 60^\circ$</th>
<th>$g = 75^\circ$</th>
<th>$g = 128^\circ$</th>
<th>$g = 128^\circ$ (with black curtains)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Cyan</td>
<td>3.9%</td>
<td>1.9%</td>
<td>1.2%</td>
<td>1.3%</td>
<td>9.0%</td>
<td>4.4%</td>
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<tr>
<td>Green</td>
<td>4.3%</td>
<td>1.9%</td>
<td>2.0%</td>
<td>2.2%</td>
<td>8.0%</td>
<td>4.1%</td>
</tr>
<tr>
<td>Red</td>
<td>1.9%</td>
<td>1.3%</td>
<td>1.4%</td>
<td>1.8%</td>
<td>2.8%</td>
<td>2.9%</td>
</tr>
<tr>
<td>Yellow</td>
<td>1.6%</td>
<td>1.3%</td>
<td>1.4%</td>
<td>1.7%</td>
<td>3.6%</td>
<td>4.6%</td>
</tr>
</tbody>
</table>
Table 3: Relative RMSE comparing spectra normalized to 754 nm from Buz et al. (2019) and TANAGER at a range of geometries for cross calibration. Green squares have RMSE <1%, yellow-green between 1% and 3% RMSE, orange between 3% and 5% RMSE, and red above 5%. “Blackout” RMSE, right, compares Buz et al. (2019) spectra to TANAGER data collected with the addition of blackout curtains in the laboratory.

<table>
<thead>
<tr>
<th>Material</th>
<th>g = 15°</th>
<th>g = 30°</th>
<th>g = 60°</th>
<th>g = 75°</th>
<th>g = 128°</th>
</tr>
</thead>
<tbody>
<tr>
<td>Cyan</td>
<td>0.4%</td>
<td>1.0%</td>
<td>0.7%</td>
<td>1.1%</td>
<td>3.5%</td>
</tr>
<tr>
<td>Green</td>
<td>0.4%</td>
<td>0.9%</td>
<td>0.6%</td>
<td>1.1%</td>
<td>4.2%</td>
</tr>
<tr>
<td>Red</td>
<td>0.3%</td>
<td>0.4%</td>
<td>0.8%</td>
<td>0.8%</td>
<td>1.1%</td>
</tr>
<tr>
<td>Yellow</td>
<td>0.3%</td>
<td>0.8%</td>
<td>0.7%</td>
<td>0.7%</td>
<td>2.1%</td>
</tr>
<tr>
<td>Gray33</td>
<td>0.2%</td>
<td>0.3%</td>
<td>0.2%</td>
<td>0.3%</td>
<td>0.9%</td>
</tr>
<tr>
<td>Gray70</td>
<td>0.3%</td>
<td>0.4%</td>
<td>0.5%</td>
<td>0.5%</td>
<td>0.5%</td>
</tr>
</tbody>
</table>

4.2 Repeatability

The repeatability of TANAGER spectra was assessed through multiple measurements of the caltarget materials at the geometries specified in Buz et al. (2019): we compared two sets of spectra collected with TANAGER in November 2022 and February 2023. The gray and black targets have residuals < 0.01 reflectance units for all spectra except at the largest phase angles, and color target spectra are generally repeatable to within 0.02 reflectance units (Figures S11-S14). To assess repeatability of spectral shapes (as opposed to absolute reflectance), we also normalized the spectra to 1.0 at 754 nm to calculate relative RMSE (as in Section 4.1). All target-geometry combinations fall well below our 5% relative RMSE threshold, with 29 of 35 target-geometry combinations below 1% RMSE (Table 4). The very forward scattering geometry is less consistent than other geometries, but overall the data show remarkable reproducibility.
Table 4: Relative RMSE comparing duplicate runs on TANAGER normalized to 754 nm for the Caltargets at a range of geometries. Green squares have RMSE <1%, yellow-green between 1% and 3% RMSE, and orange between 3% and 5% RMSE.

To test repeatability of spectral measurements of heterogeneous, geologic surfaces, we collected duplicate spectra at a range of phase angles from a set of four naturally-coated basalt samples from Hawaii Volcanoes National Park. All samples were collected from the Puna Coast and Mauna Iki Trails (Theuer et al., 2024) and all have brightly-colored coatings in a mottled pattern, except for MIT_LC, which has a more uniform reflective and chatoyant coating over fine-scaled flow textures (Figure 25). We documented the placement and orientation of each sample, which we referenced while resetting samples between the first and second set of spectra.

Figure 25: Heterogeneous, naturally-coated basalts samples used to test TANAGER’s measurement repeatability.
Figure 26: Spectra of heterogenous, naturally-coated basalt samples (PCT_RC and PCT_YC, see Figure 25) from two TANAGER data collection runs (top and middle) with residuals (bottom). All measurements were acquired at $i = 30^\circ$ and $az = 0^\circ$.

Data from the two runs reproduce the same spectral shapes and scattering behaviors: the samples are highly forward-scattering, with substantially higher reflectances and more positive near-infrared slopes at $g = 128^\circ$ (Figure 26, Figure S15). For absolute reflectance spectra,
residuals for most geometries are < 0.005 reflectance units. For spectra normalized to 1.0 at 754 nm, the two datasets have a relative RMSE of 3% or below (Table 9). The one exception is for the dark sample MIT_LC in the backscattering geometry, which has very low reflectance values (Figure S15). The reproducibility of TANAGER spectra for these samples gives us confidence in the consistency of both the spectrogoniomer’s performance and our sample staging procedure.

<table>
<thead>
<tr>
<th></th>
<th>g = 15°</th>
<th>g = 30°</th>
<th>g = 60°</th>
<th>g = 75°</th>
<th>g = 128°</th>
</tr>
</thead>
<tbody>
<tr>
<td>PCT_RC</td>
<td>0.6%</td>
<td>0.4%</td>
<td>1.0%</td>
<td>1.1%</td>
<td>0.4%</td>
</tr>
<tr>
<td>PCT_YC</td>
<td>1.5%</td>
<td>1.0%</td>
<td>1.1%</td>
<td>3.0%</td>
<td>1.1%</td>
</tr>
<tr>
<td>MIT_LC</td>
<td>5.6%</td>
<td>2.3%</td>
<td>2.1%</td>
<td>3.0%</td>
<td>2.1%</td>
</tr>
<tr>
<td>MIT_BC_2</td>
<td>2.1%</td>
<td>2.9%</td>
<td>2.2%</td>
<td>2.8%</td>
<td>0.6%</td>
</tr>
</tbody>
</table>

Table 9: Relative RMSE comparing duplicate runs on TANAGER normalized to 754 nm for four coated basalt surfaces at a range of geometries. Green squares have RMSE <1%, yellow-green between 1% and 3% RMSE, orange between 3% and 5% RMSE, and red >5% RMSE.

5. Science Applications and Data Sharing

Our preliminary science analyses have utilized TANAGER’s unique design for rapid spectral measurements for large suites of natural rock surfaces, either at a single “standard” geometry (Rice et al., 2023) or over the full scattering hemisphere (Curtis, 2022; Theuer et al., 2024). Other initial studies include characterizations of multi-phase mineral mixtures (Lapo et al., 2023) and synthetic rock coatings on slabs (Gabbert et al., 2023) and sands (Gabbert et al., 2024). Because TANAGER’s sample tray also accommodates SEM-mounted samples, we can easily correlate spectrogoniometric measurements with microtextural properties from backscattered electron (BSE) images and surface topography measurements (Duflot et al., 2022).

Ongoing work in the WWU Mars Lab will continue to exploit TANAGER’s capabilities for interrogating natural rock surfaces. More generally, we anticipate that TANAGER’s design can be useful for a variety of investigations, such as determining the bidirectional reflectance...
distribution function (BRDF) and deriving optical constants of minerals (e.g., Lucy, 1998; Sklute et al., 2015). We hope other laboratories will adapt TANAGER’s open-source design (Hoza et al., 2023) and software (Hoza, 2023) for their own niche analyses (see Data Availability Statement).

When spectral datasets from TANAGER are published in peer-reviewed studies, we will make them available via VISOR (the [V]isible and [I]nfrared [S]pectroscopy br[o]wse[r], https://westernreflectancelab.com/visor/), an online data sharing and spectra visualization tool developed by Million Concepts, LLC in partnership with the WWU Mars Lab (Million et al., 2022). VISOR allows users to search for spectra from TANAGER and/or other published spectral databases, download spectra with associated metadata (viewing geometry and sample information), and dynamically plot user-selected spectra. Plotting capabilities include adjusting axes, normalizing spectra, applying offsets, measuring selected band depths and other spectral parameters, and convolving to the bandpasses of spacecraft multispectral cameras. We will also archive all published TANAGER datasets via third party repositories (e.g., https://zenodo.org/ or https://cedar.wwu.edu/) with a digital object identifier (DOI) and persistent identifier link.

6. Conclusions

TANAGER is a custom spectrogoniometer which is fully automated and integrated with a Malvern PanAnalytical ASD FieldSpec4 Hi-Res reflectance spectrometer. We defined TANAGER’s performance requirements to enable rapid, automated spectral data collection across the full scattering hemisphere for multiple, bulky rock samples with natural surfaces. In a detailed characterization of TANAGER’s performance, all defined requirements have been met. We reevaluated a selection of the performance sub-requirements after ~300 hours of use and
found only minor changes to the system; we recommend frequent monitoring of some components, including laser guides and sample tray motors.

Using well-characterized color calibration targets, we have validated the accuracy of TANAGER spectra in comparison to published data. TANAGER spectra match those published from other spectrogoniometers within 5% relative RMSE, except for very low-albedo targets. In repeated TANAGER data collection runs for the same samples, we confirm that TANAGER spectra are self-consistent to within 2% in almost all instances. We also confirm that the system introduces no discernable noise or artifacts; in fact, TANAGER improves the polarization artifacts from ~1000 nm to 1400 nm that commonly occur in FieldSpec data at high phase angles. Furthermore, we find that TANGER’s light source causes only minimal sample heating (+2 to 4°C over typical exposure durations) and is highly unlikely to influence sample properties such as hydration state.

The advantages of TANAGER’s unique design include automation for rapid data acquisition, highly customizable viewing geometries, accommodation of multiple and/or bulky/irregular samples, and easy transfer to SEM for correlation with surface textural and compositional properties. For our near-term science analyses, TANAGER will primarily be used to characterize the surfaces of naturally-weathered rocks as analogs to the martian surface; however, TANAGER can be utilized for a variety of applications in reflectance spectroscopy. We encourage other investigators to use and/or modify TANAGER’s open-source design and software for their laboratories’ needs.
Acknowledgements

This work was funded as part of a NASA Solar System Working Program grant. We thank the staff of First Mode, LLC for their support in all stages of this project, including Peter Illsley, Elizabeth Frank and Sophia Kim. Western Washington University’s College of Science and Engineering, Geology Department, and Machine Shop supported laboratory renovations to accommodate TANAGER. We also thank Chase Million and Michael St. Clair of Million Concepts, LLC for development and ongoing support of VISOR for data sharing. Finally, we thank the Mastcam-Z instrument team for use of the caltarget witness samples.

Data Availability Statement

TANAGER’s computer-aided design (CAD), electrical schematics, and bill of materials (BOM) are publicly available as Hoza et al. (2023). TANAGER’s custom software (“tanager-feeder”), which commands its motors, interfaces with the spectrometer, and visualizes the data, is open-source and available as Hoza (2023). All spectral data acquired for TANAGER’s validation and characterization are available as Lapo et al. (2024).

References


J.F. Bell III, A. Godber, S. McNair, M.C. Caplinger, J.N. Maki, M.T. Lemmon, et al., The Mars Science Laboratory Curiosity rover Mast Camera (Mastcam) instruments: pre-


Shaw, A., Daly, M. G., Cloutis, E., Basic, G., Hamilton, D., Tait, K., et al. (2016). Reflectance properties of grey-scale Spectralon® as a function of viewing angle,


Introduction

Here we present details of the characterization of the Three-Axis N-sample Automated Goniometer for Evaluating Reflectance (TANAGER) instrument upon delivery to Western Washington University (WWU) in Spring 2021. These characterization data (Text S1-S5) were collected to evaluate TANAGER's performance requirements (Table 1 in the main text), and later to reevaluate them after ~300 hours of instrument use (Table S1). From these assessments we have developed recommendations for long-term TANAGER operations (Text S6).
Text S1. Sample Heating Characterization

Incident light sources can gradually raise the temperature of illuminated portion of samples, which may cause signal drift (change in spectral shape and reflectance over time), loss of adsorbed water (especially for particulate samples) and/or phase changes for some minerals. To quantify these effects, we measured sample temperature and spectral changes over one hour of exposure to the TANAGER light source for solid and particulate targets with a range of albedos: Spectralon® white reference target (Labsphere Inc.; Sutton, New Hampshire), Gray70 color standard (70% white, Lucideon Inc.), Gray33 color standard (33% white, Lucideon Inc.), Black color standard (Lucideon Inc.), basalt sand (Columbia River Flood Basalts, Grand Ronde; 125-250 μm), and powdered kieserite (Sigma-Aldrich).

The temperature of each target was collected just before exposure to incident light and then at regular intervals over the next hour using an infrared laser thermometer with +/- 0.1°C accuracy. Spectralon® and Lucideon Black were also exposed to the incident light source of a Malvern Panalytical Contact Probe for comparison. The distance from light source to target is not equivalent for TANAGER (22 cm) and the Contact Probe (3.5 cm), nor are the illumination sources (the Contact Probe uses a halogen bulb and TANAGER uses a stabilized broadband tungsten-halogen light source), but given that the Contact Probe is an industry standard for geologic sample characterization, it provides a useful point of comparison.

We evaluated target temperatures after two, ten, and 60 minutes of exposure to the incident light source as typical illumination durations during TANAGER data collection (two minutes is the duration each sample remains under the illuminated spot during an automated run). All samples heated rapidly immediately after exposure to incident light. Beyond ten minutes, samples continued heating at a slower rate until a maximum temperature was reached over the next hour (Figure S2). Targets increased by 2-4°C after two minutes of exposure to the TANAGER light source and up to 16°C after an hour, except for Spectralon®, which heated negligibly (0.4°C). These temperature increases are not insignificant, but they are a noticeable improvement over those from the Contact Probe (Figure 22). We observed no changes to the reflectance spectra for any targets over the duration of the experiment.

Text S2. Heating and Dehydration Characterization

We exposed crushed anhydrite (CaSO₄, also known as drierite, powdered to < 106 μm) to the TANAGER light source and monitored spectral changes as a test for whether enough heating would occur to drive off adsorbed water. We ran one experiment for 30 minutes of intermittent light exposure (in 2-3 minute cycles, which simulates normal use of TANAGER), and another for 30 minutes of continuous exposure (which simulates maximum exposure during TANGER setup). During both tests, we collected spectra every
We observed minimal changes to the temperature of the anhydrite under intermittent and continuous exposure to incident light. Under intermittent exposure, the temperature increased by a maximum of 0.7°C from baseline. Under continuous exposure, the temperature increased by 2.4°C in the first 5 minutes, and an additional 0.7°C after the full 30 minutes of the experiment. These continuous exposure results are consistent with our other heating experiments (Text S1).

We also observed negligible spectral changes during both experiments (Figure S3). The spectra of powdered anhydrite are bright and largely featureless, except for the hydration features at ~1400 nm and ~1900 nm. The smaller features near 1750 nm and 2210 nm indicate that minor gypsum (CaSO\textsubscript{4} \cdot 2H\textsubscript{2}O) is present in the sample, and therefore some component of the hydration features is attributable to structural water; however, most of the band depths near 1400 nm and 1900 nm are attributable to adsorbed water molecules on the mineral grains.

We measured band depths beneath a continuum (Clark & Roush, 1984) for the absorptions at 1420 nm and 1910 nm during exposure to TANAGER’s light source (Figure S4). Band changes negligible during both the intermittent (less than 0.0005 over 30 minutes) and continuous exposure experiments (<0.006 for both bands, with ~90% of the change occurring within the first 10 minutes). These results suggest very minor changes to the amount of adsorbed water on the powered samples, which gives us confidence that heating due to TANAGER’s light source will not drive off significant adsorbed water from mineral grains or otherwise dehydrate samples during normal operations.

Overall, we assess that the TANAGER light source is low risk for inducing spectral changes, but we still recommend caution where appropriate. Continuous exposure can be limited by taking care to keep the incident light on the Spectralon® puck (which has negligible temperature effects; Figure S2) or a blank sample slot, instead of a target sample, during set up and between data collection runs. Additionally, during height finding (which usually occurs under the incident light), the light source can be turned off.

Text S3. Detector Spot Size Characterization

We determined TANAGER’s detector spot size by collecting spectra of a series of black paper disks with central openings of increasing diameter layered over white paper. The disks were 7 cm in diameter and had apertures that ranged from 1 to 5 cm. We made disks with apertures at intervals of 0.2 cm from 1.0 to 3.0 cm, and 0.5 cm from 3.0 to 5.0
We collected spectra at $e = 0^\circ$, $15^\circ$, $30^\circ$, $50^\circ$, and $70^\circ$; and $i = 0^\circ$ (except for $e = 0^\circ$, where we instead used $i = 30^\circ$).

We evaluated spectra between 635 nm and 1395 nm (where the black paper has a steep positive slope, and the white paper has a near-zero slope) using two metrics: slope and root mean square error (RMSE), a statistical comparison of similarity between series. RMSE is calculated using the following formula:

$$RMSE = \sqrt{\frac{\sum_{i=1}^{n}(P - O)^2}{n}}$$

where $P$ is the predicted value (or reflectance of the white paper) and $O$ is the observed value (or reflectance of the disk). Disks with neutral slopes and low RMSE indicate a lack of influence from the black paper and an aperture size larger than the detector spot size.

A high and a low confidence threshold were used to provide a range of slope and RMSE values considered similar to white paper based on the natural variation in 4 spectra of the white paper. The high confidence threshold was determined by:

$$\text{MAX white paper} + (\text{MAX white paper} - \text{MIN white paper})$$

where MAX white paper is the maximum slope or RMSE value from the 4 white paper spectra and MIN white paper is the minimum slope or RMSE value. The low confidence threshold is similarly calculated by:

$$\text{MAX white paper} + [5*(\text{MAX white paper} - \text{MIN white paper})]$$

Spectra of disks that yield RMSE or slope values below these thresholds are considered to lack influence from the black disk, indicating that the spot size is smaller than the aperture for that disk.

Spot sizes at a range of geometries are shown in Table 2 in the main text. The low end of the reported spot size range is the smallest diameter based on RMSE and slope where the black paper does not influence the spectrum based on the low confidence threshold. The high end of the reported spot size range is the same based on the high confidence threshold. Spot sizes range from $<1.6$ cm at $e = 0^\circ$ to $<3.5$ cm at $e = 70^\circ$.

**Text S4. Vibration Characterization**

Vibration caused by TANAGER could cause samples to shift, resulting in changes in the field of view over the duration of a run, either from particulate material settling over time or from variations in light source or detector pointing due to vibration. To assess the baseline vibration from TANAGER, we used the *Vibration Analysis* mobile phone application (Kharutskiy, 2014). All measurements were taken with a phone placed on
TANAGER’s sample tray, except “Lab bench” (Figure S4), which was collected with the phone on the lab bench as a baseline for the lab’s vibration. We assessed the following possible sources of vibration: TANAGER itself while still; TANAGER incidence, azimuth, and sample tray movement; and the slamming of self-closing fire doors adjacent to the lab. We measured vibration at a sampling rate of 100 Hz in the units of g. The intensity of vibration is reported as the minimum value for a measurement subtracted from the maximum value.

All measurements except azimuth movement and tray movement yielded vibration intensity less than the resolution of the measurements (0.018g based on the software and hardware limitations; Allan, 2011), which we consider to be negligible. Tray movement vibration intensity is up to 3x the data resolution (0.057g in the x-axis), and azimuth movement intensity is up to 12x the data resolution (0.221g in the y-axis) (Figure S4). These values are still considered low and since neither movement happens during data collection, the likelihood of impact is low.

Repeat imagery of mixed particulate material in a TANAGER sample cup further confirms that TANAGER movements are unlikely to shift materials and negatively impact the quality and consistency of spectra (Figure S6). Spectral repeatability of variable surfaces in Section 4.2 also suggests that pointing and illumination are consistent and not affected by instrument vibration.

Text S5: Polarization Artifact Characterization

TANAGER design parameters require that polarization artifact peaks at ~1100 and 1300 nm (Section 2.7) are less than 0.1 reflectance for dark basalt samples. Since delivery, TANAGER data has rarely shown these artifacts and, qualitatively, peaks are diffuse and muted compared to data collected with the contact probe or with spectrometers comparable to the FieldSpec.

We evaluated these polarization artifacts (Section 2.7, Figure 18) for TANAGER spectra using a full hemispheric dataset of coated basalts from Hawai’i. The artifacts were not visible in most spectra, but some of those at larger phase angles displayed clear artifacts with peaks at ~1100 and 1300 nm (Figure S7). We quantified the difference between polarization artifacts and the continuum by dividing the maximum difference between measured values and a continuum by the continuum value at that wavelength. Percent differences are between 0.76% and 2.15%, with slightly lower differences for the 1100 nm peaks than the 1300 nm peaks. All measured percent differences, therefore, are well below the 10% threshold required by TANAGER parameters and are qualitatively rare and small in TANAGER data. Therefore, we do not consider polarization artifacts to be an ongoing concern in our datasets.
Text S6: Recommendations for Long-Term TANAGER Operations

After two years and more than 300 hours of use, we reevaluated a selection of TANAGER’s requirements (Table 1) for data quality, alignment of key parts, and consistency of movement. We compared results to the initial assessments performed by First Mode, LLC on delivery of TANAGER in the spring of 2021, and found that most requirements are still met (Table S1). The only hardware aspect with measurable degradation was the consistency in sample tray positioning, which varied an average of 0.8 mm with a maximum variability of 1.8 mm (a considerable increase from values on delivery). Higher errors resulted from “jerky” movements of the sample tray, which we attribute to degradation of its motor.

We also found that the accuracy of the intersecting lasers on the incidence arm (that indicate the plane of measurement) can shift over time. These lasers had no quantitative design requirements, but we evaluated them after ~250 hours of TANAGER run time when one of the lasers needed replacement. It is unclear how significant laser shift is over time, but due to their importance for sample positioning, we recommend recalibrating the lasers periodically to ensure they intersect in the center of the incidence light footprint and 11” above the baseplate, and before long (> 1 day) runs or before datasets intended for publication.

In summary, we recommend reevaluating most performance requirements every 300-500 hours, and more frequently for the lasers, sample tray repeatability, and other items as concerns arise. When any components are replaced (e.g., light source, motors), the relevant performance requirements should be evaluated promptly.
Figure S1. Examples of shadows cast by TANAGER’s detector for phase angles $g=10^\circ$ (a-b) and $g=20^\circ$ (c). The requirement that the detector head not fall inside the incident light beam for $g \geq 20^\circ$ (sub-requirement 1.1, Table 1) is not met, as shown in (c), but we find this to be acceptable because the shadowed region is outside the detector pointing.
Figure S2. Changes in temperature under TANAGER’s incident light source for a range of solid and particulate targets. Changes in temperature under a Malvern Panalytical Contact Probe for the Spectralon® and Black color standard are shown for comparison.
Figure S3: Fifteen spectra of anhydrite (CaSO₄) acquired over 30 minutes of continuous exposure to TANAGER’s incident light source. Prominent absorption bands due to hydration are labeled. No meaningful changes to these absorptions (or any other spectral features) were observed during heating experiments, implying that TANAGER’s light source is unlikely to drive off adsorbed water from mineral grains (or otherwise dehydrate samples).
Figure S4: Changes to hydration band depths due to adsorbed water on anhydrite grains during continuous exposure to TANAGER’s light source. Above: 1420 nm band depth beneath a continuum with shoulders at 1330 nm and 1500 nm; Below: 1910 nm band depth beneath a continuum with shoulders at 1820 nm and 2050 nm.
Figure S5: Total variation (maximum – minimum acceleration values) for x, y and z axes yielded from possible TANAGER vibration sources. The dashed horizontal line represents the resolution of the hardware and software.

Figure S6: A mixture of loose gravel and grass in a TANAGER sample cup before and after being subjected to a full 360° rotation of the sample tray in 60° increments; and 360° of azimuth rotation (0° to 180° and 180° back to 0°).
Figure S7: Spectra of a coated basalt from Hawaii with minor polarization artifacts at 1100 nm and 1300 nm.
Figure S8: Spectra of the AluWhite and yellow Mastcam-Z caltarget witness samples at multiple viewing geometries from TANAGER (top) compared to Buz et al. (2019) (middle), with residuals (bottom). All measurements were acquired at $i = 30^\circ$ and $az = 0^\circ$. 

TANAGER, 2022

Buz et al., 2019

Buz et al. - TANAGER
Figure S9: Spectra of the green and dark gray (33% white) Mastcam-Z caltarget witness samples at multiple viewing geometries from TANAGER (top) compared to Buz et al. (2019) (middle), with residuals (bottom). All measurements were acquired at $i = 30^\circ$ and $az = 0^\circ$. 
Figure S10: Spectra of color caltargets collected with TANAGER in a very forward-scattering geometry \((g = 128^\circ)\) with and without blackout curtains on the lab cabinetry (“Blackout” vs. “Standard”). The curtains reduce stray light reflected from lab surfaces and reduce overall reflectance (but do not otherwise change spectral shape). Spectra are offset for clarity (Cyan by -0.55; Green by -0.15; Red by +0.40; Yellow by +0.80).
Figure S11: Spectra of the cyan and red Mastcam-Z caltarget witness samples from two TANAGER data collection runs (top and middle) with residuals (bottom). All measurements were acquired at $i = 30^\circ$ and $az = 0^\circ$. 
Figure S12: Spectra of the light gray (70% white) and black Mastcam-Z caltarget witness samples from two TANAGER data collection runs (top and middle) with residuals (bottom). All measurements were acquired at $i = 30^\circ$ and $az = 0^\circ$. 
Figure S13: Spectra of the dark gray (33% white) and AluWhite Mastcam-Z caltarget witness samples from two TANAGER data collection runs (top and middle) with residuals (bottom). All measurements were acquired at $i = 30^\circ$ and $az = 0^\circ$. 
Figure S14: Spectra of the green and yellow Mastcam-Z caltarget witness samples from two TANAGER data collection runs (top and middle) with residuals (bottom). All measurements were acquired at $i = 30^\circ$ and $az = 0^\circ$. 
Figure S15: Spectra of heterogenous, naturally-coated basalt samples (MIT_LC and MIT_BC, see Figure 25) from two TANAGER data collection runs (top and middle) with residuals (bottom). All measurements were acquired at i = 30° and az = 0°.
<table>
<thead>
<tr>
<th>Requirement</th>
<th>Reevaluation</th>
<th>Recommendation</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.11 Signal drift from heating at small phase angles</td>
<td>Standard deviation is less than 0.005 over 15 minutes of exposure to incident light</td>
<td>Reevaluate every 300-500 hours of use, and when a new bulb is installed</td>
</tr>
<tr>
<td>1.12 Noise</td>
<td>Noise values &lt; 0.001 at all wavelengths (quantified by subtracting an original spectrum from its Savitzky-Golay smoothed spectrum; window size = 19, order = 2)</td>
<td>Reevaluate every 300-500 hours of use</td>
</tr>
<tr>
<td>1.13 Polarization artifacts</td>
<td>Measured &lt; 0.01 difference in reflectance from artifact to continuum (or as high as 2.2% of the continuum)</td>
<td>Reevaluate every 300-500 hours of use</td>
</tr>
<tr>
<td>1.3 Angular control</td>
<td>All angular controls have an accuracy &lt;1°:</td>
<td>Reevaluate every 300-500 hours of use</td>
</tr>
<tr>
<td></td>
<td>• Incidence: 0.3° average, 0.8° max variability</td>
<td></td>
</tr>
<tr>
<td></td>
<td>• Emission: 0.3° average, 0.9° max variability</td>
<td></td>
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<tr>
<td></td>
<td>• Azimuth: &lt;0.1° average, 0.1° max variability</td>
<td></td>
</tr>
<tr>
<td>1.5 Pointing accuracy - light source</td>
<td>Illumination pointing to varies with azimuth motion by 1.0 mm - 1.6 mm (4% - 6% of incidence spot size)</td>
<td>Reevaluate every 300-500 hours of use</td>
</tr>
<tr>
<td>1.6 Pointing accuracy - detector</td>
<td>Detector spot deviates from the target point by 4.5% of the detector spot size diameter</td>
<td>Reevaluate every 300-500 hours of use</td>
</tr>
<tr>
<td>2.3 Sample tray repeatability</td>
<td>Average repeatability of 0.8 mm and a maximum variability of 1.8 mm</td>
<td>Reevaluate every ~100 hours to assess for further motor degradation</td>
</tr>
</tbody>
</table>

**Table S1.** Summary of TANAGER requirements that were reevaluated after ~300 hours of instrument use, with recommendations for how often they should be revisited in long-term operations. Details of requirements are given in Table 1.